



# **Faculty of Automotive and Construction Machinery Engineering**

WARSAW UNIVERSITY OF TECHNOLOGY

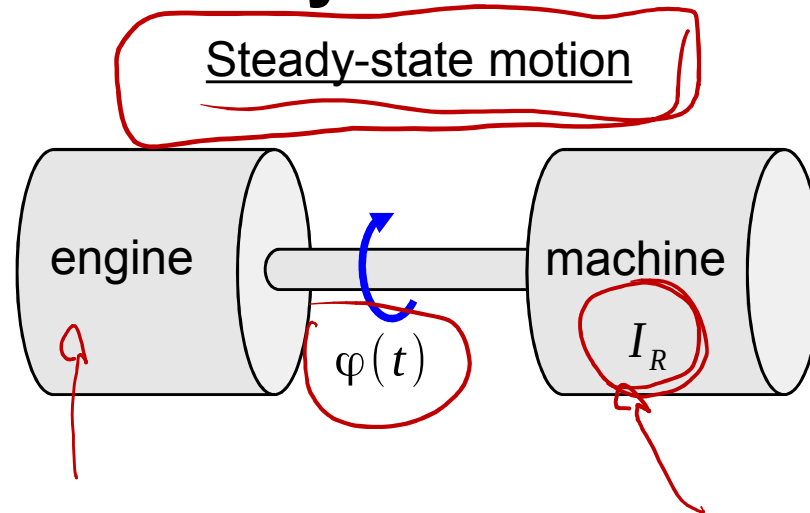
## ***Theory of Machines and Automatic Control*** Winter 2019/2020

**Lecturer: Sebastian Korczak, PhD Eng.**

# Lecture 7

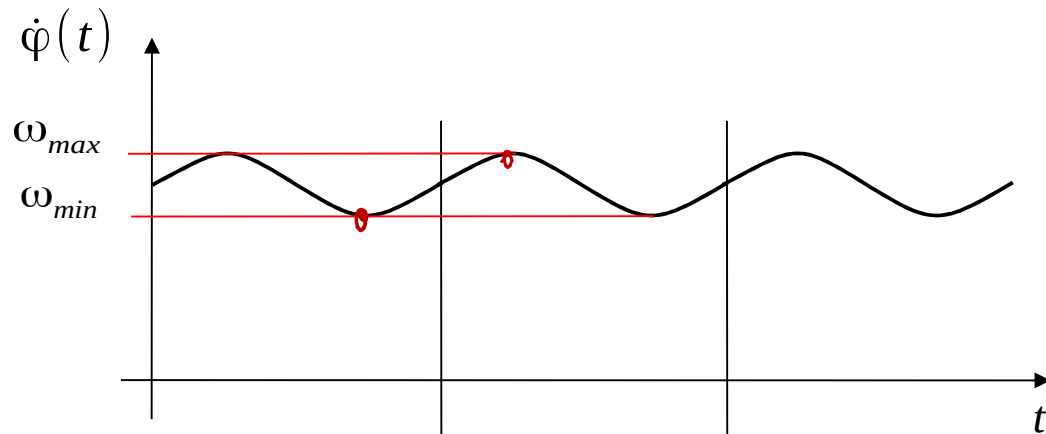
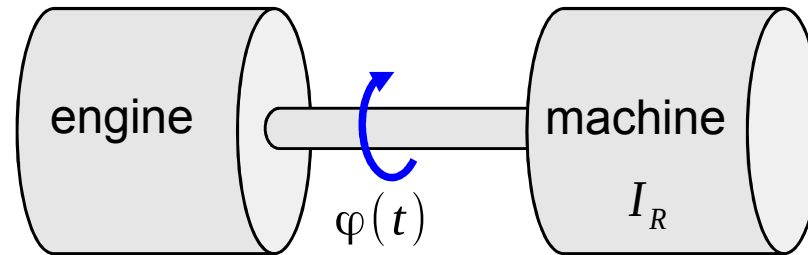
Non-uniformity of machine motion.  
Introduction to automatic control.

# Non-uniformity of machine motion



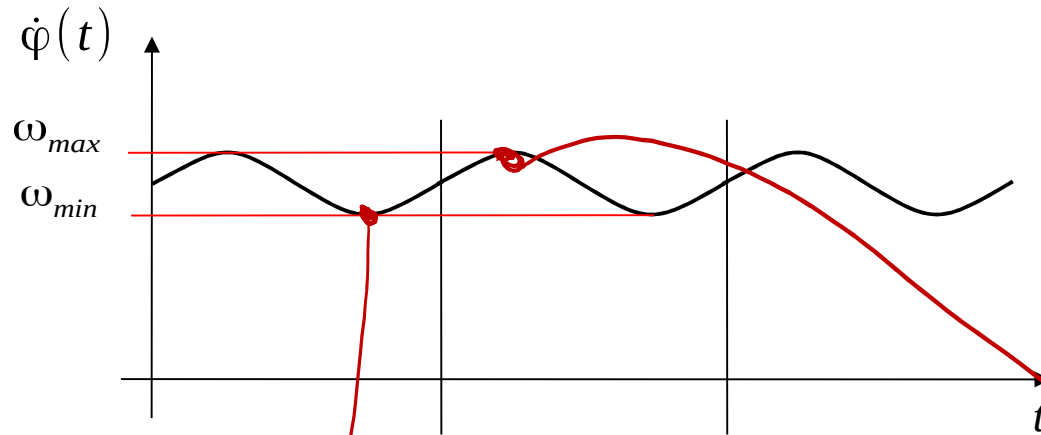
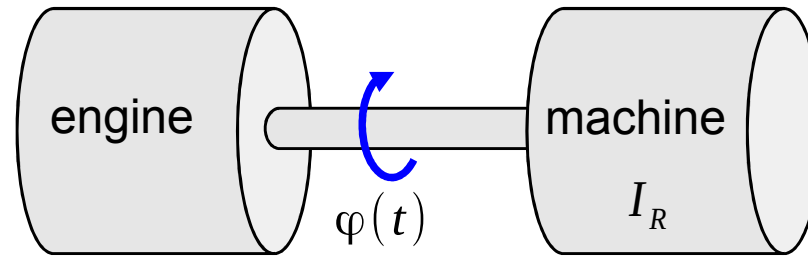
# Non-uniformity of machine motion

Steady-state motion



# Non-uniformity of machine motion

Steady-state motion



Non-uniformity of machine motion

$$\delta = \frac{\omega_{max} - \omega_{min}}{\omega_{mean}}$$

$$\omega_{mean} = \frac{\omega_{max} + \omega_{min}}{2}$$

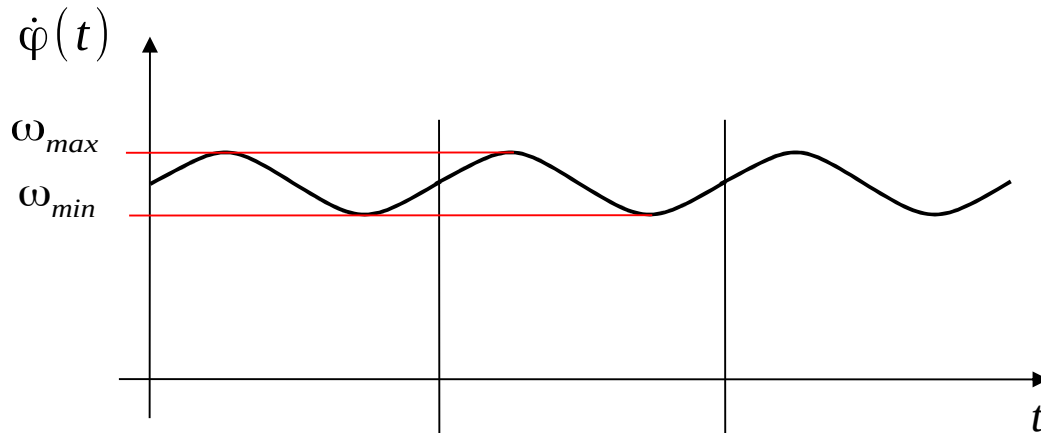
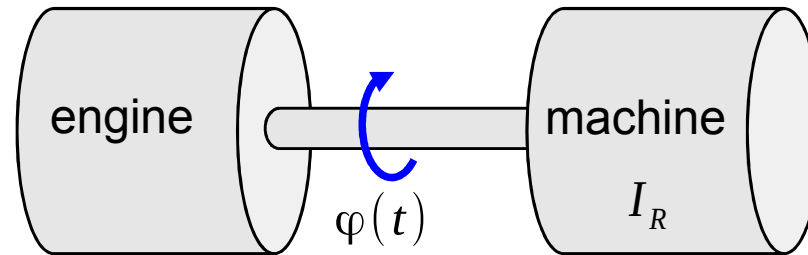
$$T_{min} = \frac{1}{2} I_R \omega_{min}^2$$

$$T_{max} = \frac{1}{2} I_R \omega_{max}^2$$

$$W = T_{max} - T_{min} = \frac{1}{2} I_R (\omega_{max}^2 - \omega_{min}^2) = \delta I_R \omega_{mean}^2$$

# Non-uniformity of machine motion

Steady-state motion



Non-uniformity of machine motion

$$\delta = \frac{\omega_{max} - \omega_{min}}{\omega_{mean}} \quad \omega_{mean} = \frac{\omega_{max} + \omega_{min}}{2}$$

pumps

$$\delta = \underline{1/5} \div 1/30$$

combustion engines

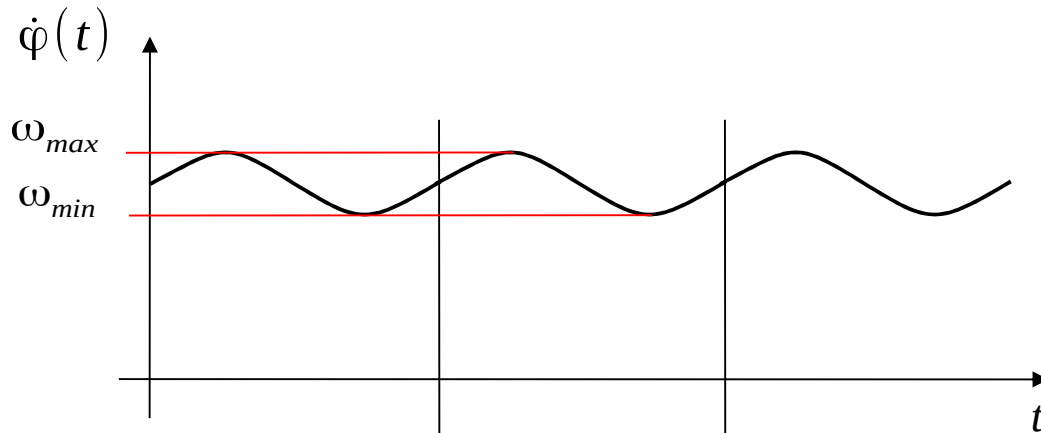
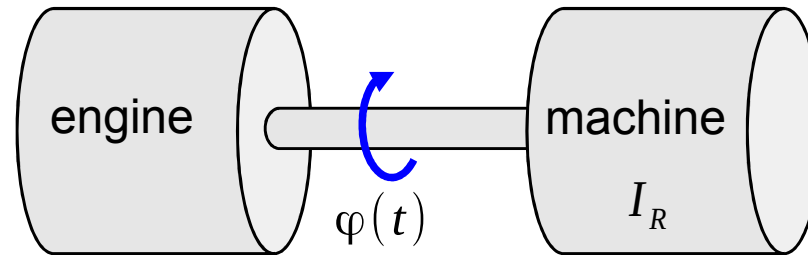
$$\delta = 1/50 \div 1/150$$

generators

$$\delta = 1/200 \div 1/300$$

# Non-uniformity of machine motion

Steady-state motion



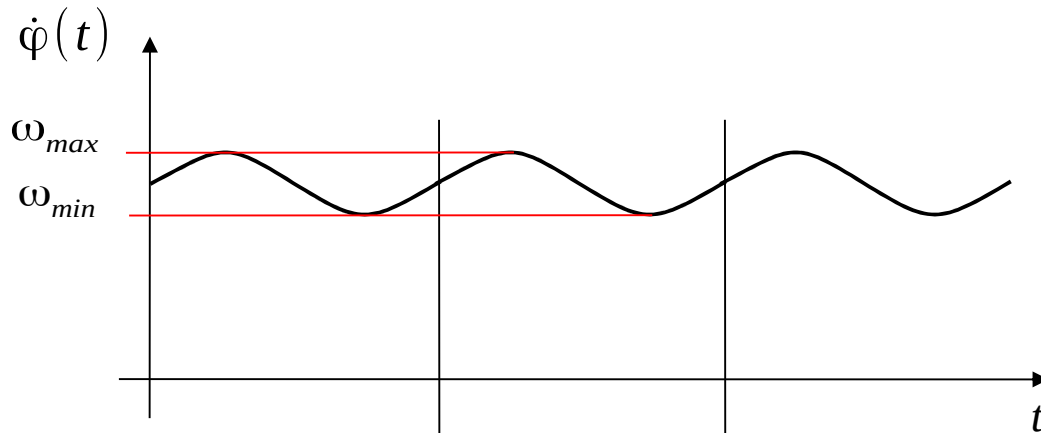
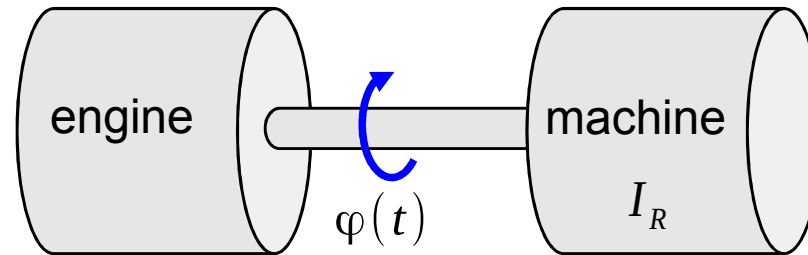
Non-uniformity of machine motion

$$\delta = \frac{\omega_{max} - \omega_{min}}{\omega_{mean}} \quad \omega_{mean} = \frac{\omega_{max} + \omega_{min}}{2}$$

$$T_{max} = \frac{1}{2} I_R \omega_{max}^2 \quad T_{min} = \frac{1}{2} I_R \omega_{min}^2$$

# Non-uniformity of machine motion

Steady-state motion



Non-uniformity of machine motion

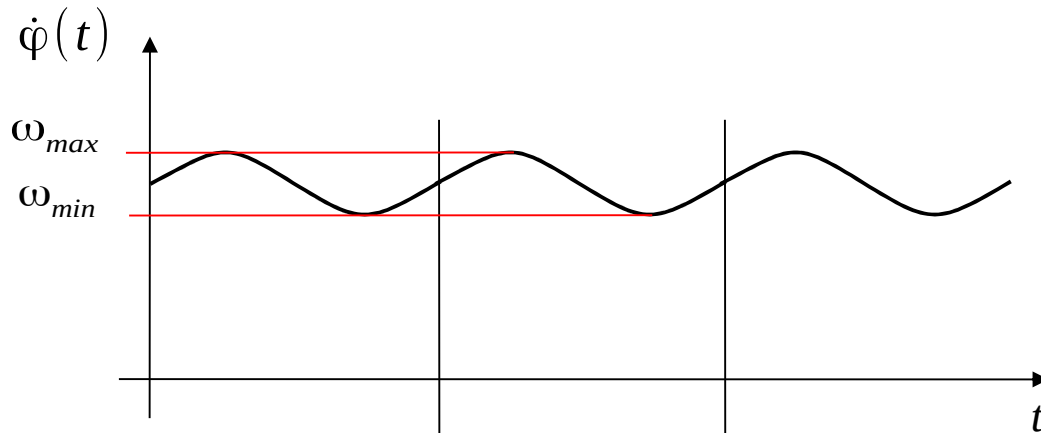
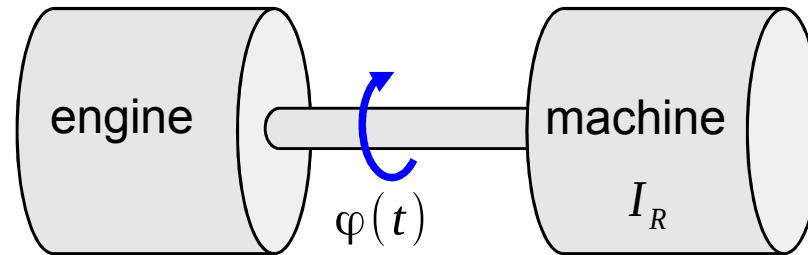
$$\delta = \frac{\omega_{max} - \omega_{min}}{\omega_{mean}} \quad \omega_{mean} = \frac{\omega_{max} + \omega_{min}}{2}$$

$$T_{max} = \frac{1}{2} I_R \omega_{max}^2 \quad T_{min} = \frac{1}{2} I_R \omega_{min}^2$$

$$W = T_{max} - T_{min}$$

# Non-uniformity of machine motion

Steady-state motion



Non-uniformity of machine motion

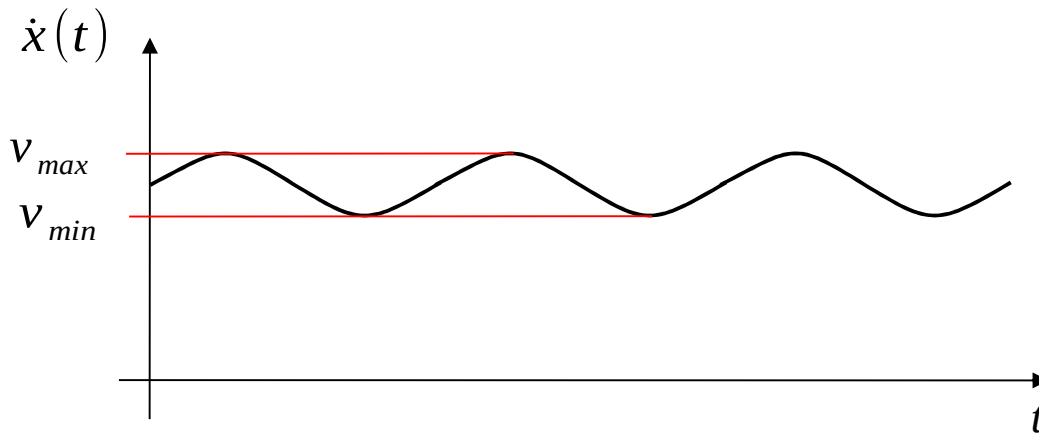
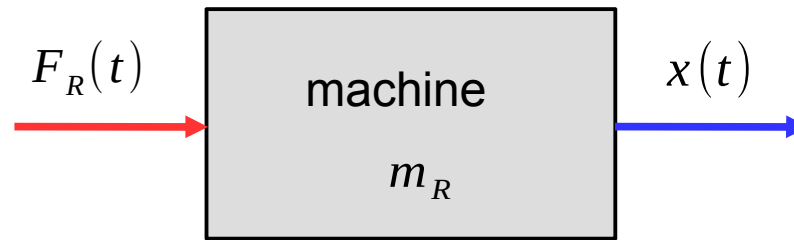
$$\delta = \frac{\omega_{max} - \omega_{min}}{\omega_{mean}} \quad \omega_{mean} = \frac{\omega_{max} + \omega_{min}}{2}$$

$$T_{max} = \frac{1}{2} I_R \omega_{max}^2 \quad T_{min} = \frac{1}{2} I_R \omega_{min}^2$$

$$W = T_{max} - T_{min} = \delta I_R \omega_{mean}^2$$

# Non-uniformity of machine motion

Steady-state motion



Non-uniformity of machine motion

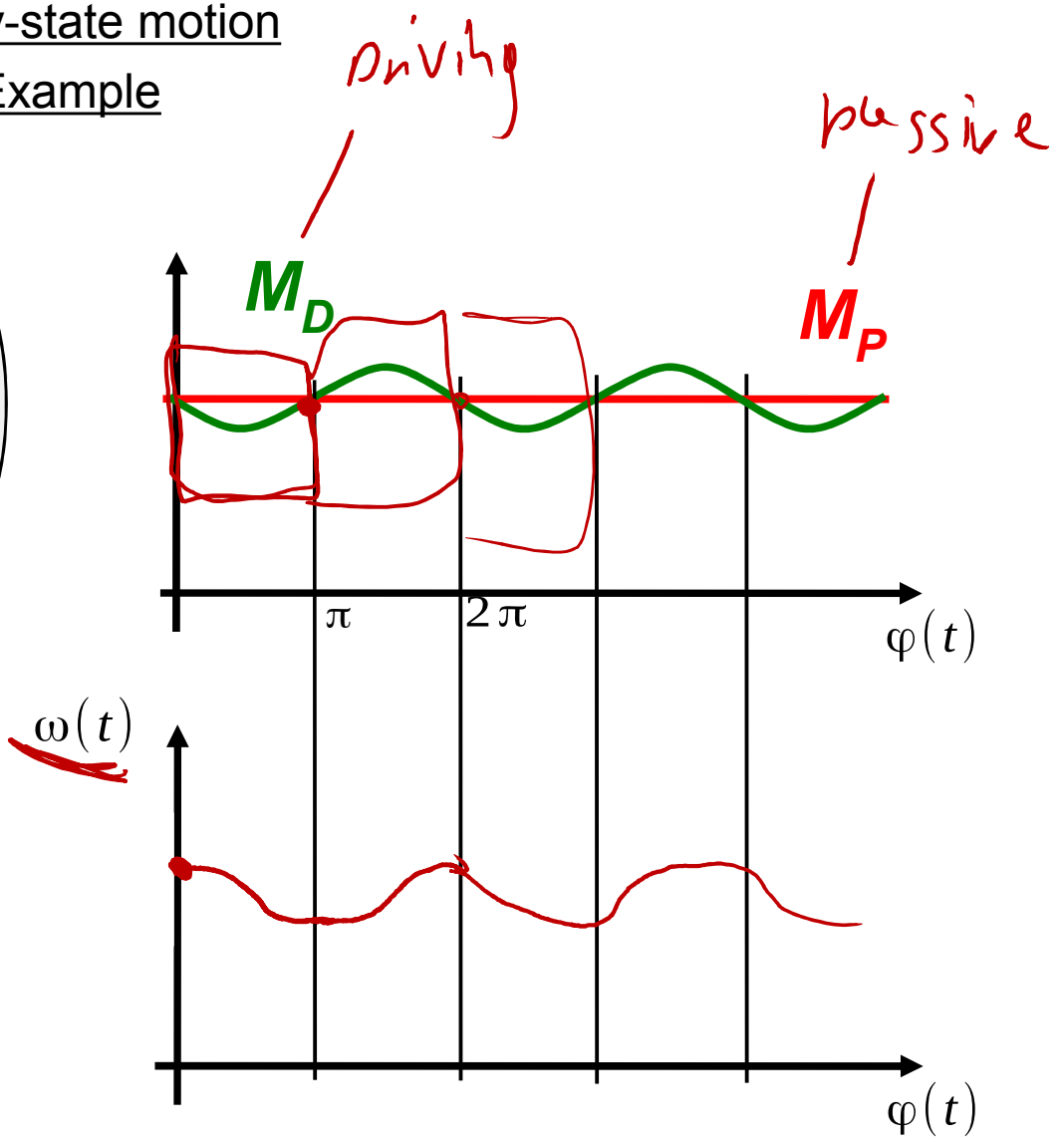
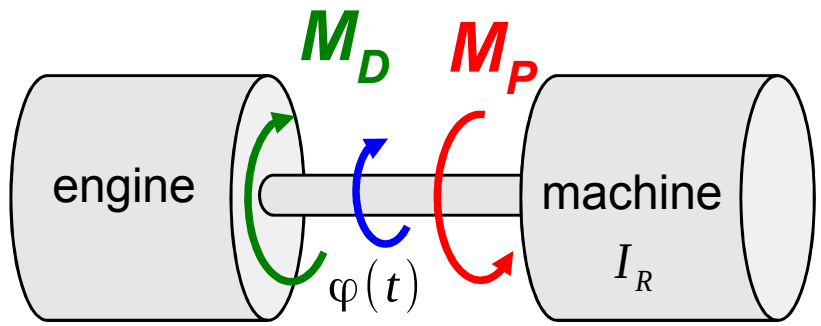
$$\delta = \frac{v_{max} - v_{min}}{v_{mean}} \quad v_{mean} = \frac{v_{max} + v_{min}}{2}$$

$$W = \delta m_R v_{mean}^2$$

# Non-uniformity of machine motion

Steady-state motion

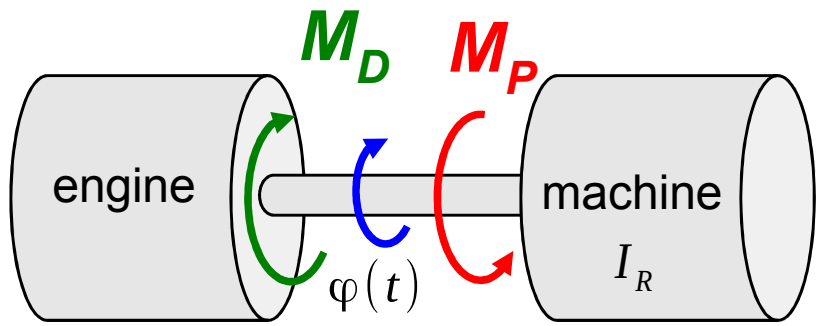
Example



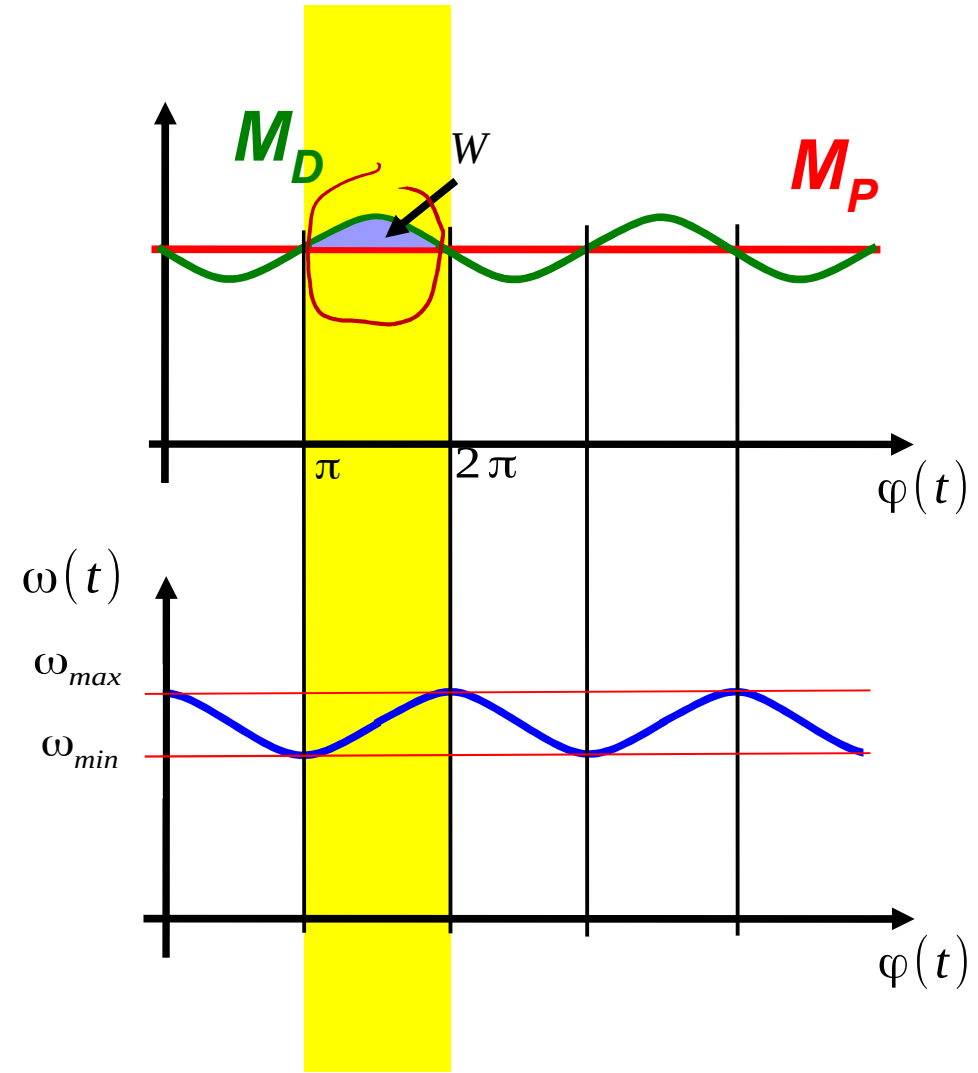
# Non-uniformity of machine motion

Steady-state motion

Example



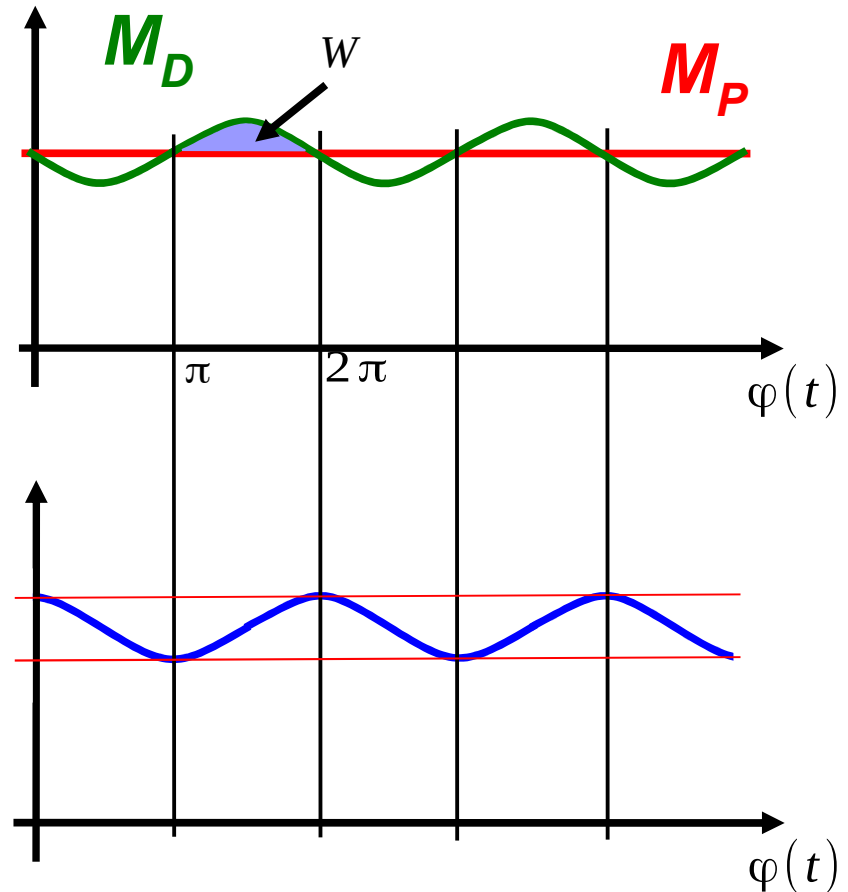
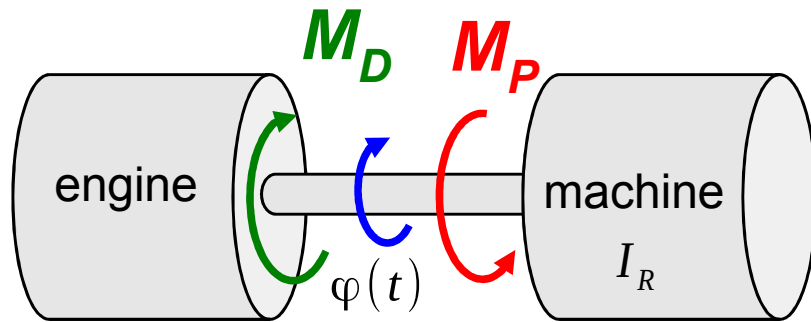
$$W = \int_{\varphi_{min}}^{\varphi_{max}} (M_D - M_P) d\varphi$$



# Non-uniformity of machine motion

Steady-state motion

Example



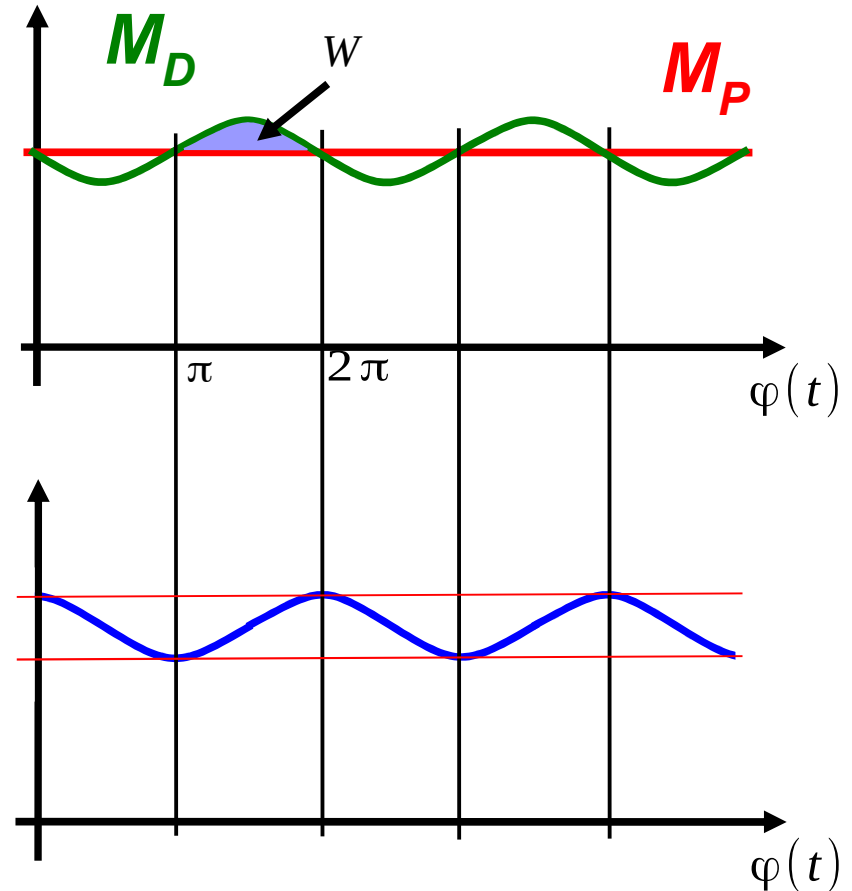
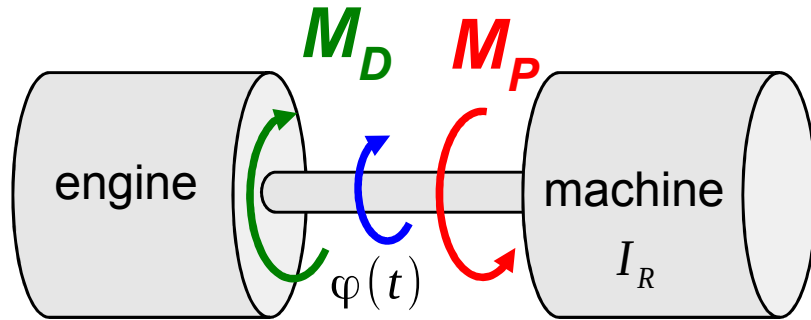
$$W = \int_{\varphi_{min}}^{\varphi_{max}} (M_D - M_P) d\varphi$$

$$W = T_{max} - T_{min} = \delta I_R \omega_{mean}^2$$

# Non-uniformity of machine motion

Steady-state motion

Example



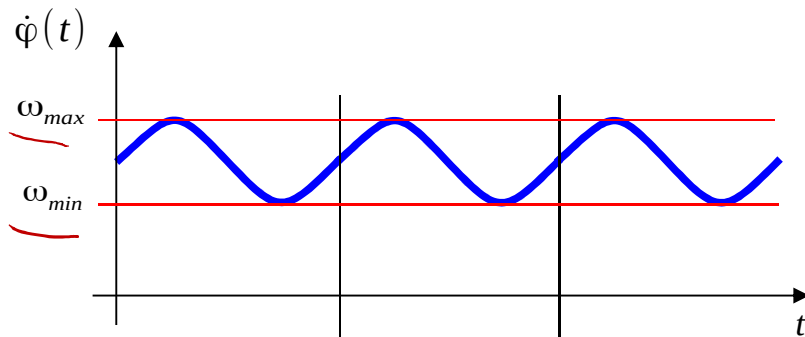
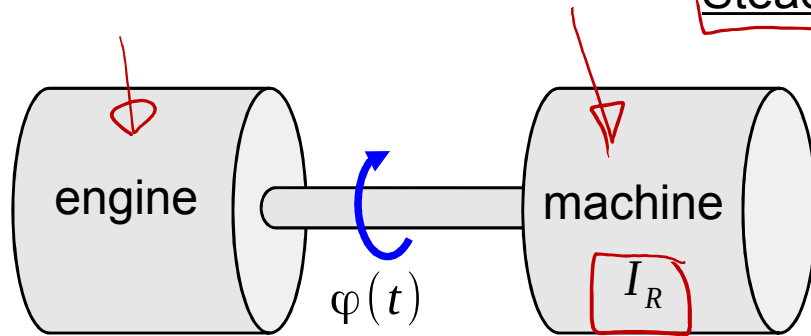
$$W = \int_{\varphi_{min}}^{\varphi_{max}} (M_D - M_P) d\varphi$$

$$W = T_{max} - T_{min} = \delta I_R \omega_{mean}^2$$

$$\delta = \frac{W}{I_R \omega_{mean}^2}$$

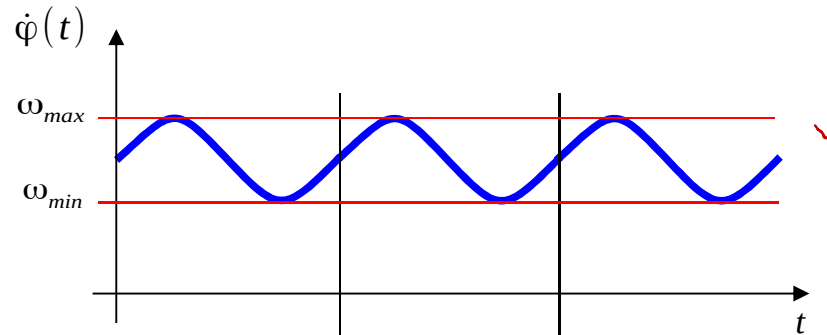
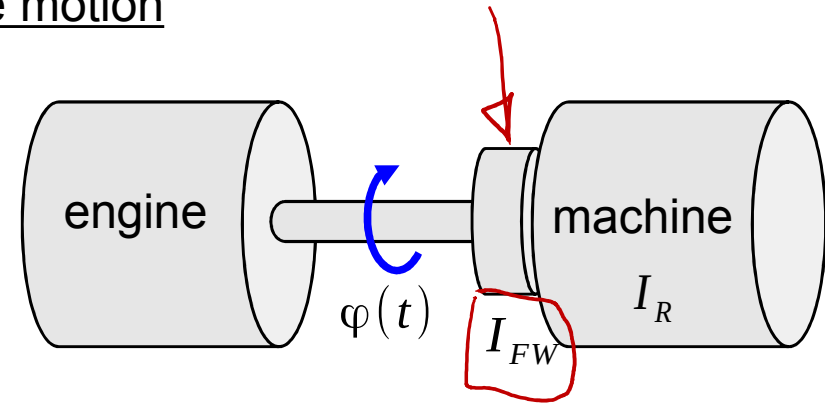
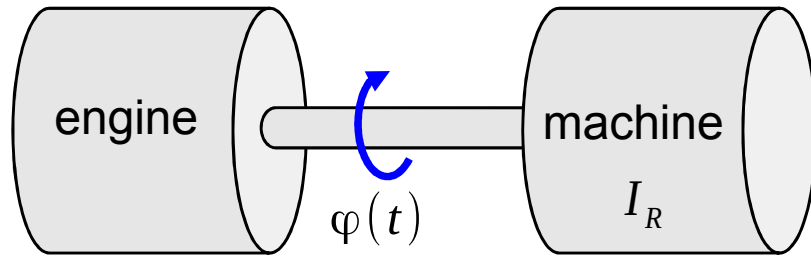
# Flywheel

Steady-state motion



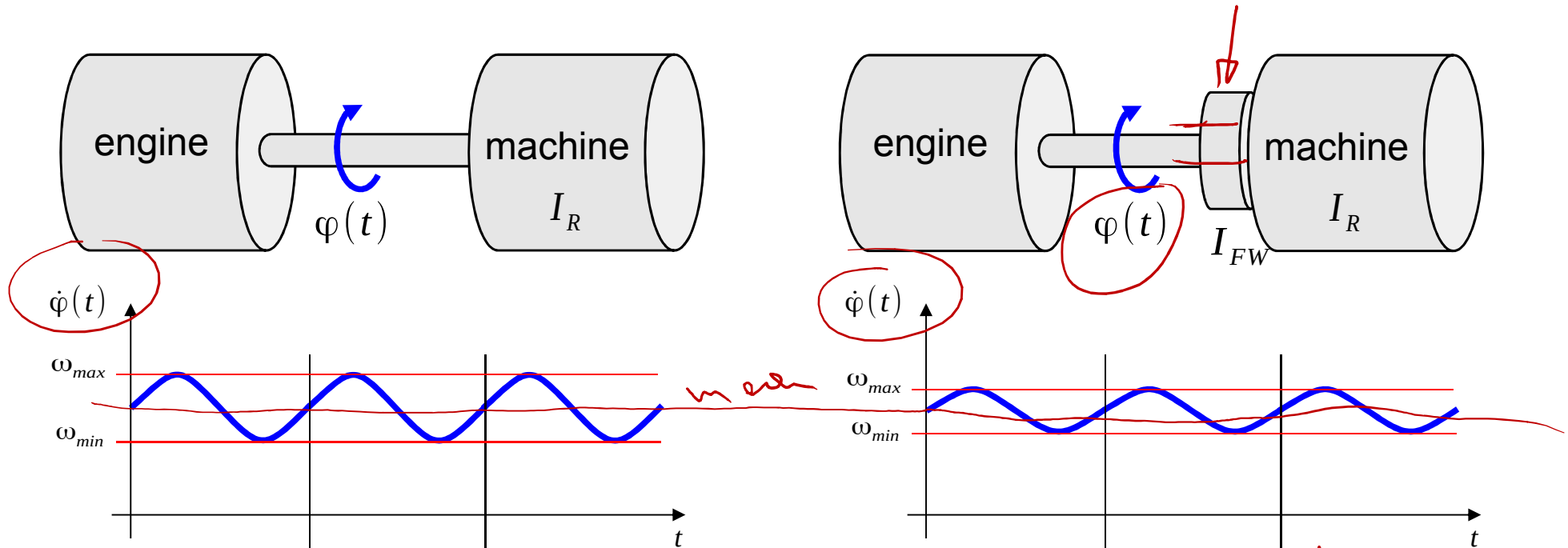
# Flywheel

## Steady-state motion



# Flywheel

## Steady-state motion



$$W_1 = \delta_1 I_R \omega_{mean}^2$$

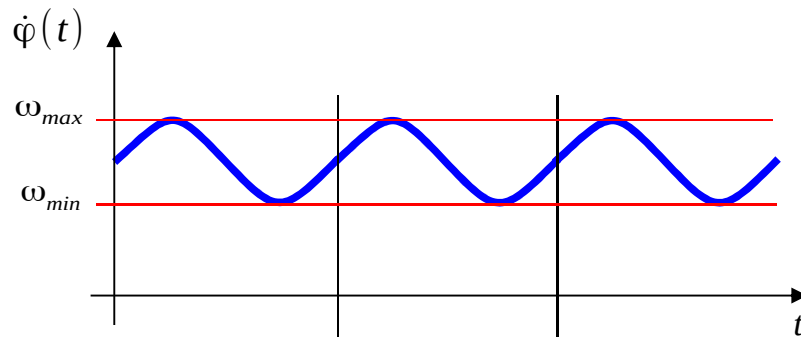
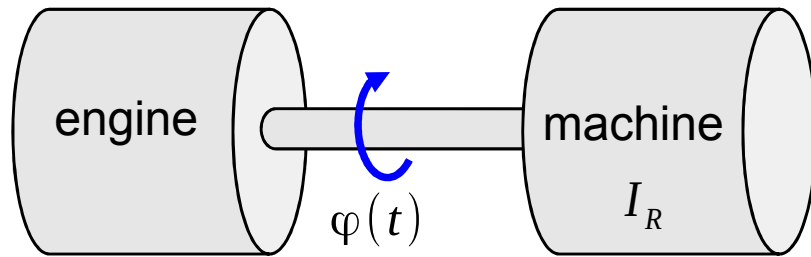
$$W_2 = \delta_2 (I_R + I_{FW}) \omega_{mean}^2$$

$$W_1 = W_2 \rightarrow \delta_1 I_R \omega_{mean}^2 = \delta_2 (I_R + I_{FW}) \omega_{mean}^2$$

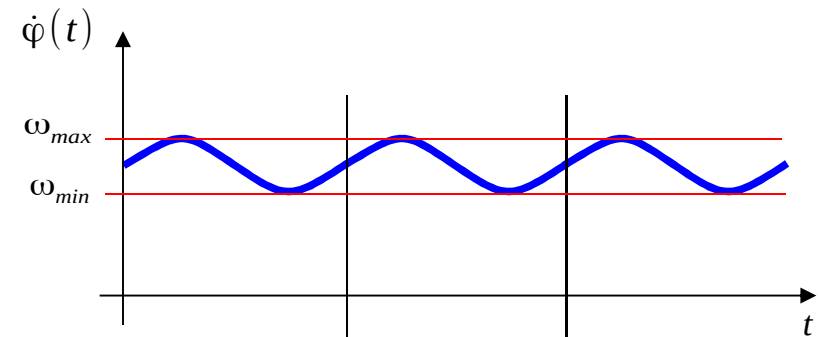
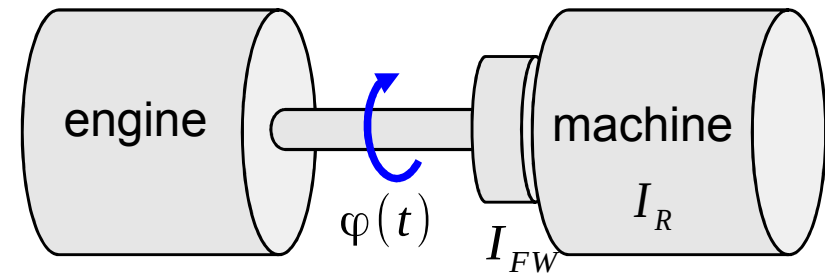
$$I_{FW} = \left( \frac{\delta_1}{\delta_2} - 1 \right) I_R$$

# Flywheel

## Steady-state motion



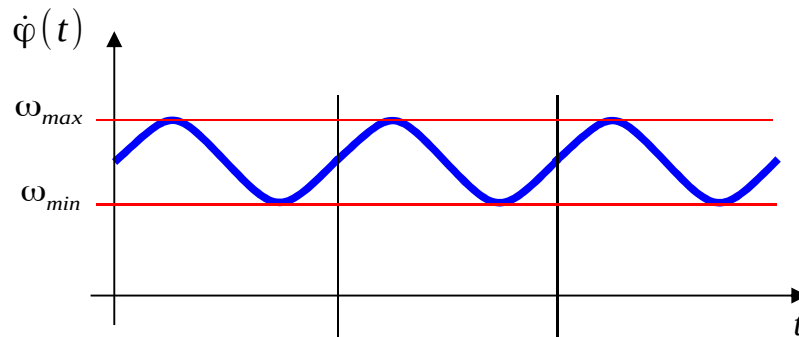
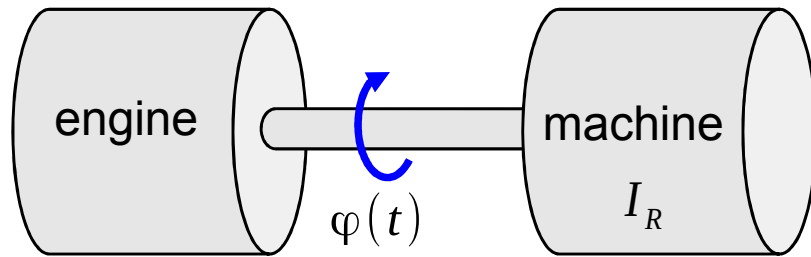
$$W = \delta_1 I_R \omega_{mean}^2$$



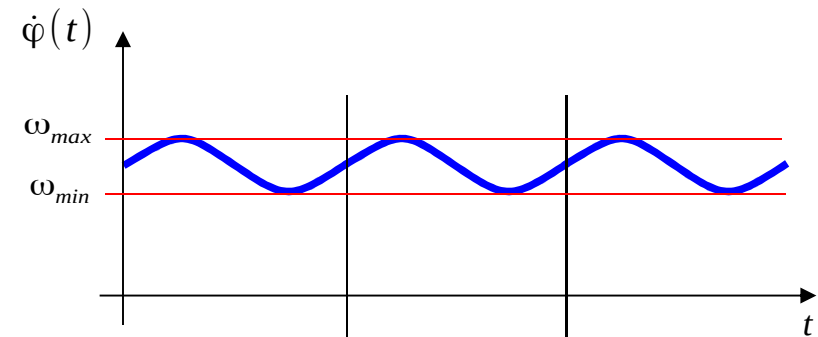
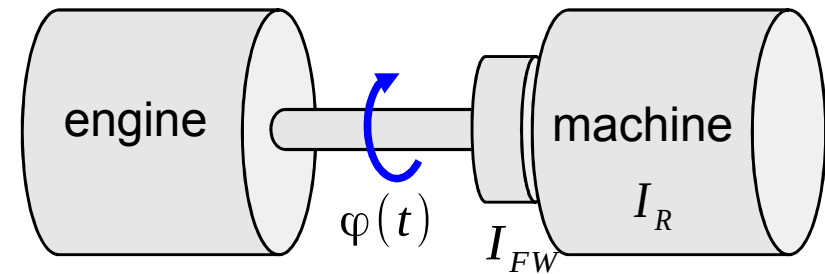
assume  
 $I_R \approx const.$

# Flywheel

## Steady-state motion



$$W = \delta_1 I_R \omega_{mean}^2$$



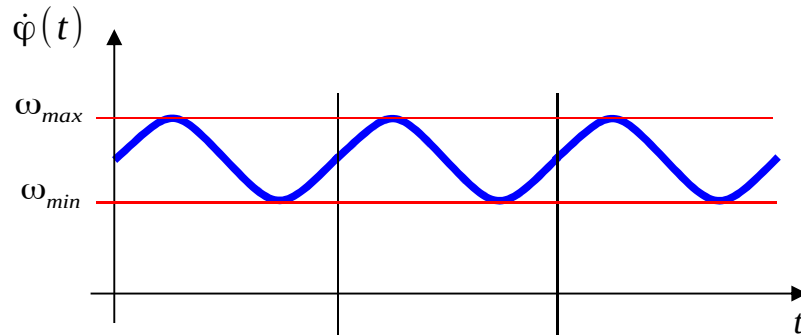
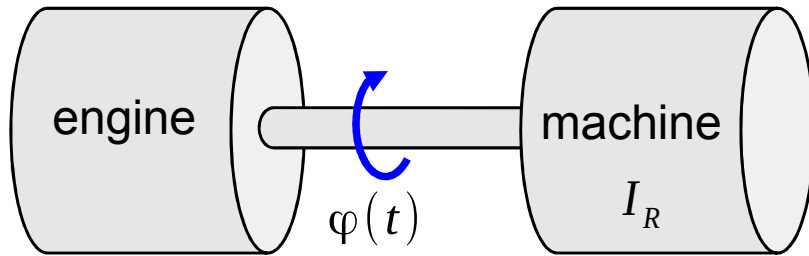
assume  
 $I_R \approx const.$

$$W = \delta_2 (I_R + I_{FW}) \omega_{mean}^2$$

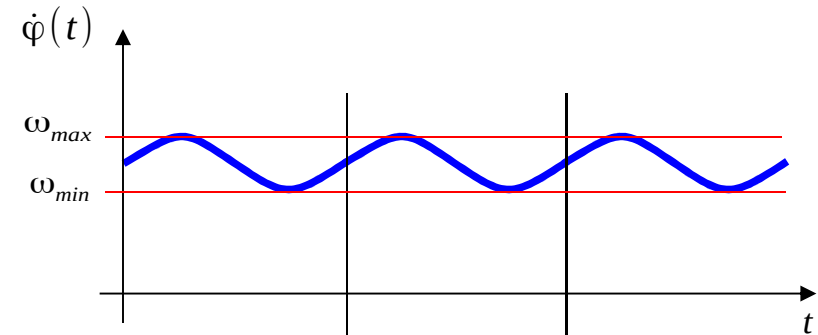
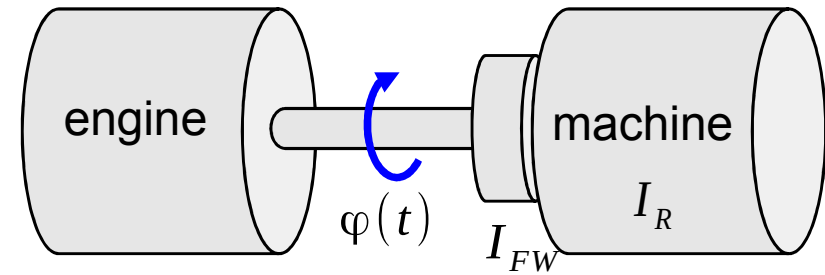
(if velocity of a flywheel  
same as analyzed velocity)

# Flywheel

## Steady-state motion



$$W = \delta_1 I_R \omega_{mean}^2$$



assume

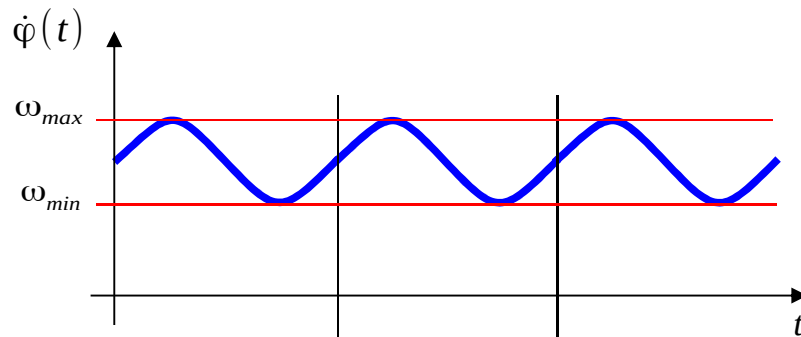
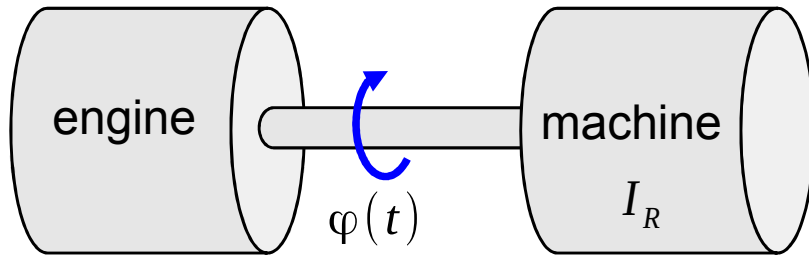
$I_R \approx const.$

$$W = \delta_2 (I_R + I_{FW}) \omega_{mean}^2$$

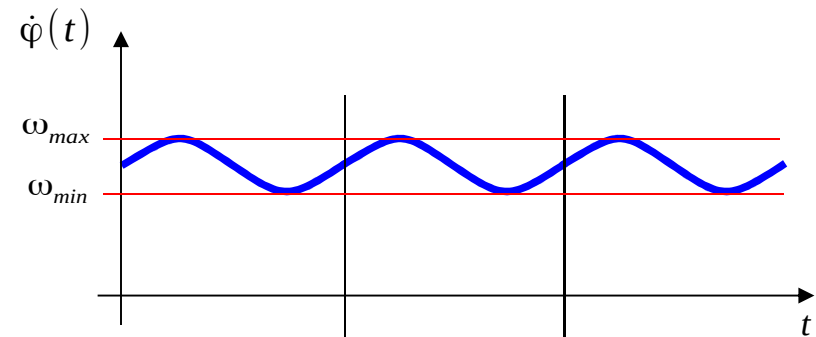
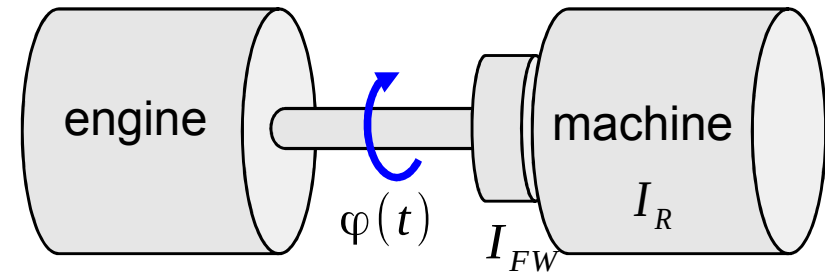
$$\delta_1 I_R \omega_{mean}^2 = \delta_2 (I_R + I_{FW}) \omega_{mean}^2$$

# Flywheel

## Steady-state motion



$$W = \delta_1 I_R \omega_{mean}^2$$



assume

$$I_R \approx const.$$

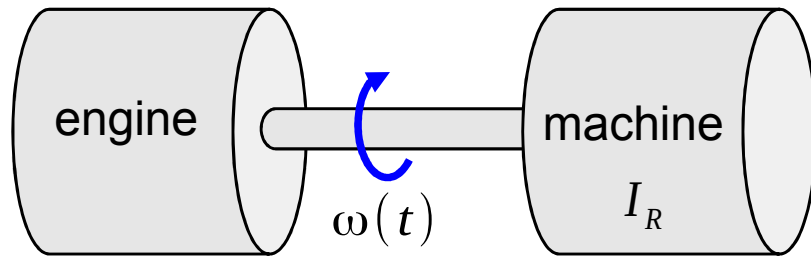
$$W = \delta_2 (I_R + I_{FW}) \omega_{mean}^2$$

$$\delta_1 I_R \omega_{mean}^2 = \delta_2 (I_R + I_{FW}) \omega_{mean}^2$$

$$I_{FW} = \left( \frac{\delta_1}{\delta_2} - 1 \right) I_R$$

# Non-uniformity of machine motion

## Example 1



Given:

$$\omega_{max}(t) = 1000 \text{ rpm}$$

$$\omega_{min}(t) = 950 \text{ rpm}$$

$$I_R = 10 \text{ kgm}^2$$

Design flywheel to obtain 10rpm velocity variations.

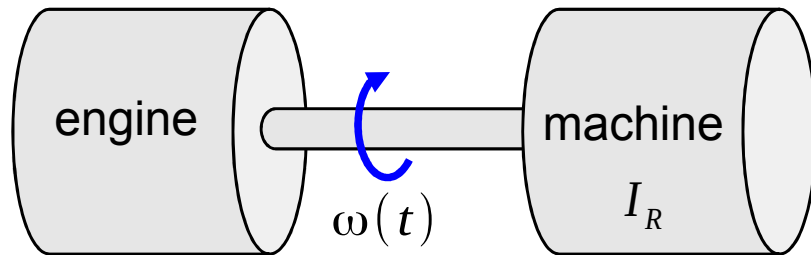
$$\text{WITHOUT F.W. : } \delta = \frac{\omega_{max} - \omega_{min}}{\omega_{mean}} = \frac{50 \text{ rpm}}{975 \text{ rpm}}$$

$$\text{WITH F.W. : } \delta_{FW} = \frac{10 \text{ rpm}}{975 \text{ rpm}}$$

$$I_{FW} = \left( \frac{\delta}{\delta_{FW}} - 1 \right) I_R = 4 I_R = 40 \text{ kgm}^2$$

# Non-uniformity of machine motion

## Example 1



Given:

$$\omega_{max}(t) = 1000 \text{ rpm}$$

$$\omega_{min}(t) = 950 \text{ rpm}$$

$$I_R = 10 \text{ kgm}^2$$

Design flywheel to obtain 10rpm velocity variations.

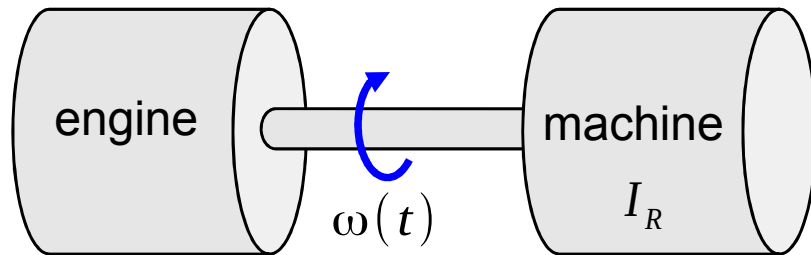
Non-uniformity without a flywheel:

Desired non-uniformity with a flywheel:

Mass moment of inertia of a flywheel:

# Non-uniformity of machine motion

## Example 1



Given:

$$\omega_{max}(t) = 1000 \text{ rpm}$$

$$\omega_{min}(t) = 950 \text{ rpm}$$

$$I_R = 10 \text{ kgm}^2$$

Design flywheel to obtain 10rpm velocity variations.

Non-uniformity without a flywheel:

$$\delta = \frac{\omega_{max} - \omega_{min}}{\omega_{mean}} = \frac{50}{975} = 0,0513$$

Desired non-uniformity with a flywheel:

$$\delta_{FW} = \frac{10}{975} = 0,010256$$

Mass moment of inertia of a flywheel:

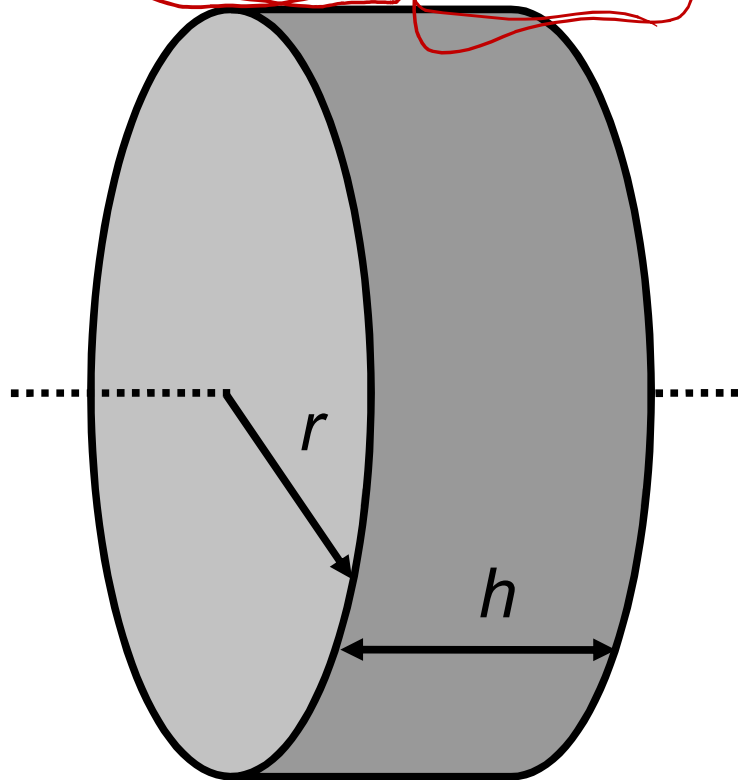
$$I_{FW} = \left( \frac{\delta}{\delta_{FW}} - 1 \right) I_R = 40 \text{ kg m}^2$$

# Non-uniformity of machine motion

## Example 1

Solid cylinder

$$I_{FW} = \frac{1}{2} m r^2 = \frac{1}{2} \rho \pi h r^4$$



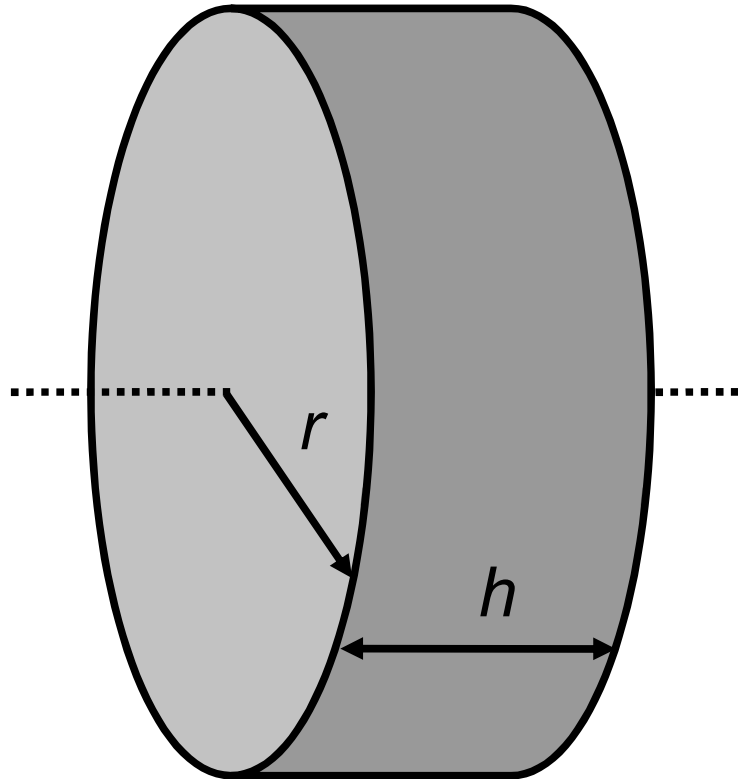
$\rho$  - density

# Non-uniformity of machine motion

## Example 1

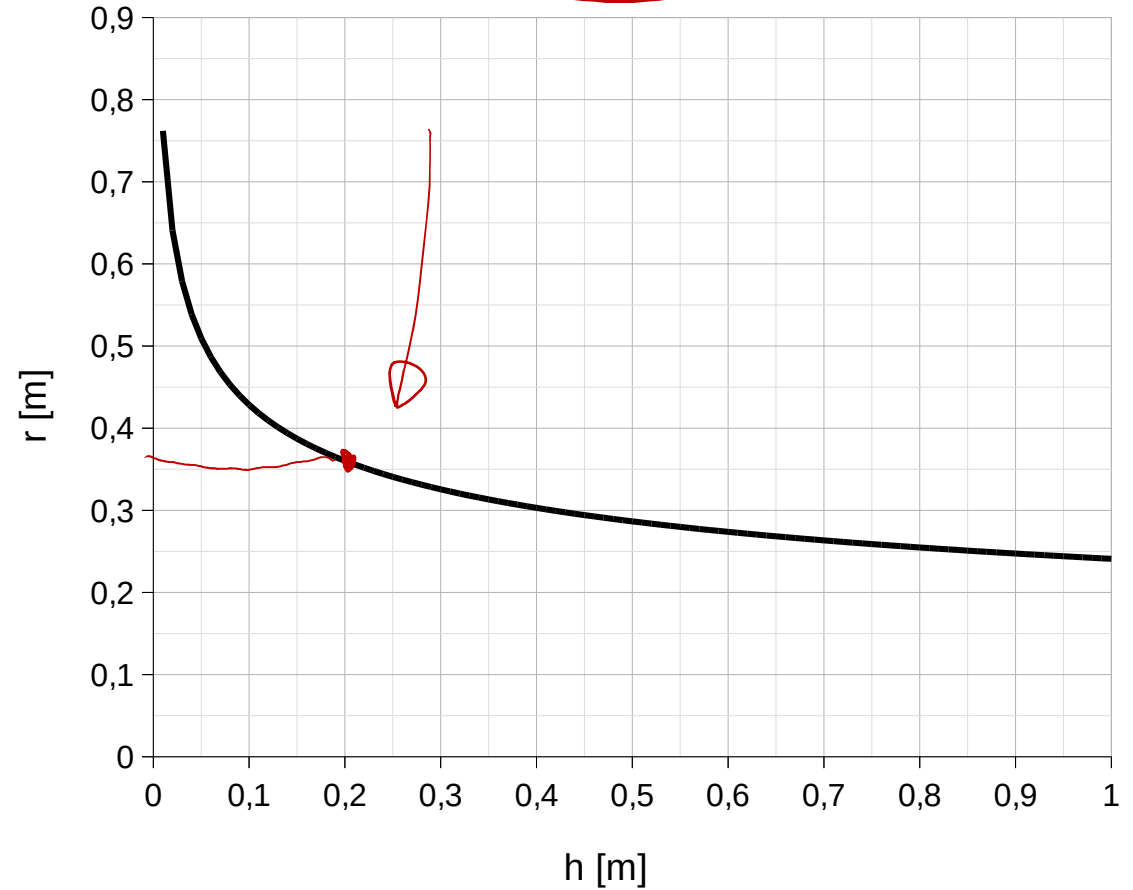
Solid cylinder

$$I_{FW} = \frac{1}{2} m r^2 = \frac{1}{2} \rho \pi h r^4$$



$$I_{FW} = 40 \text{ kgm}^2$$

$$\rho_{\text{steel}} = 7800 \text{ kg/m}^3$$



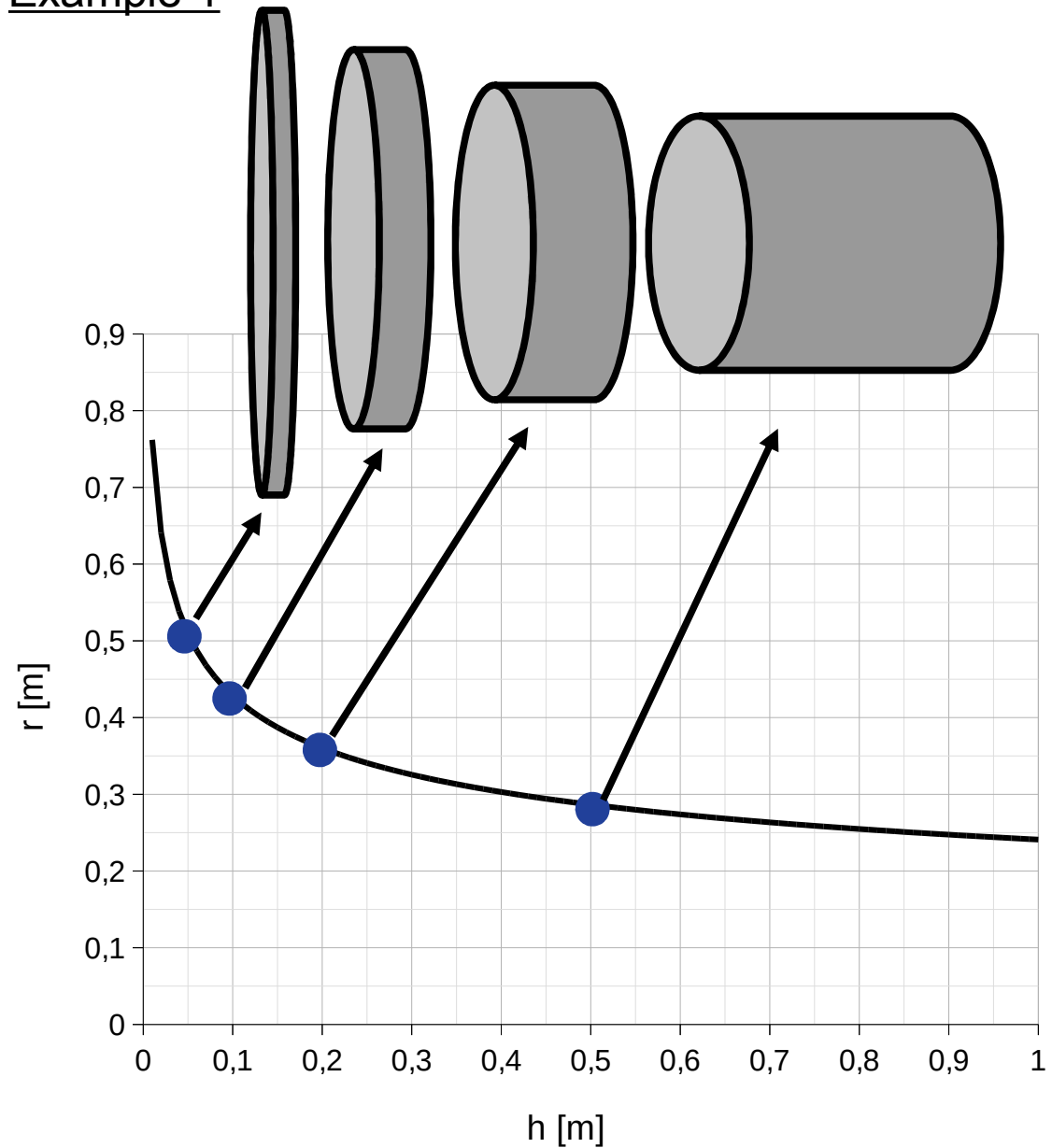
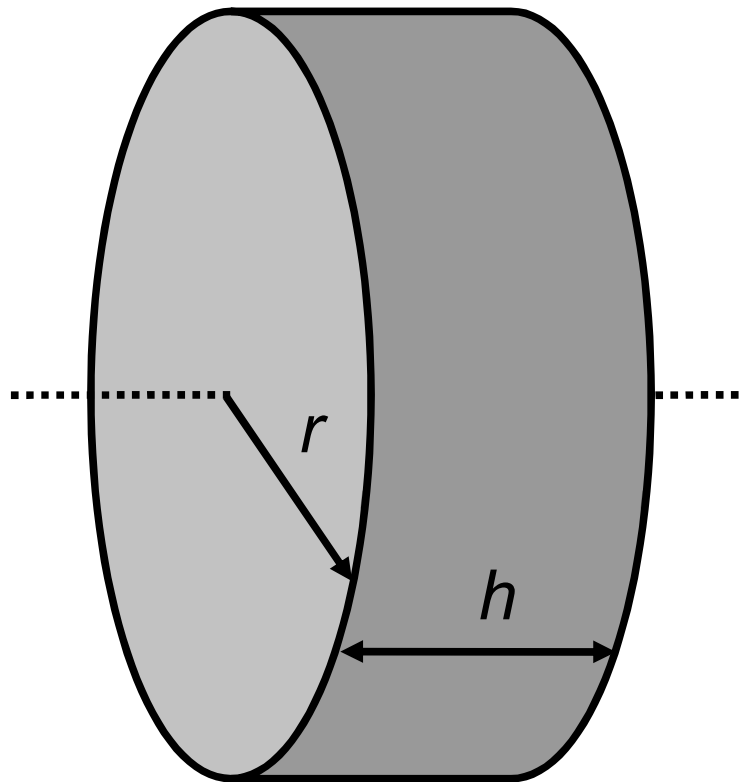
# Non-uniformity of machine motion

## Example 1

Solid cylinder

$$I_{FW} = \frac{1}{2} m r^2 = \frac{1}{2} \rho \pi h r^4 = 40 \text{ kgm}^2$$

$$\rho_{steel} = 7800 \text{ kg/m}^3$$



# Non-uniformity of machine motion

Example 1

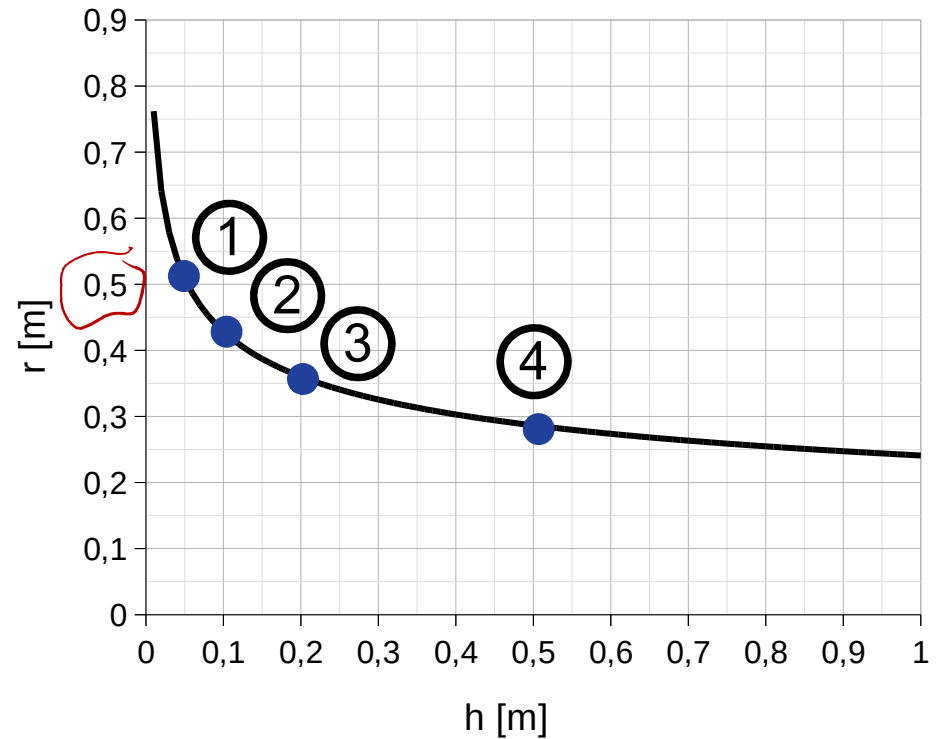
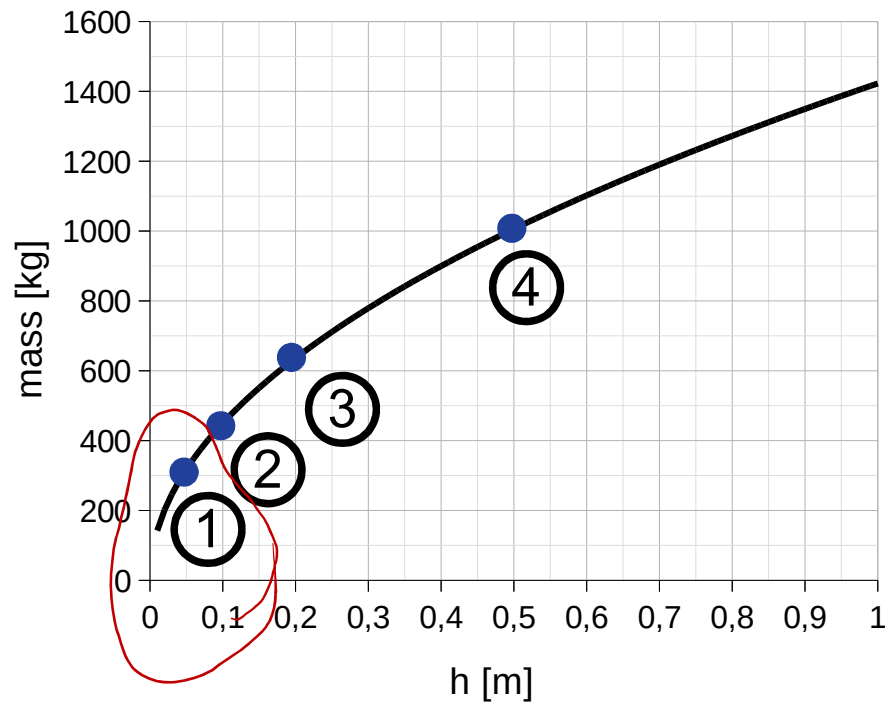
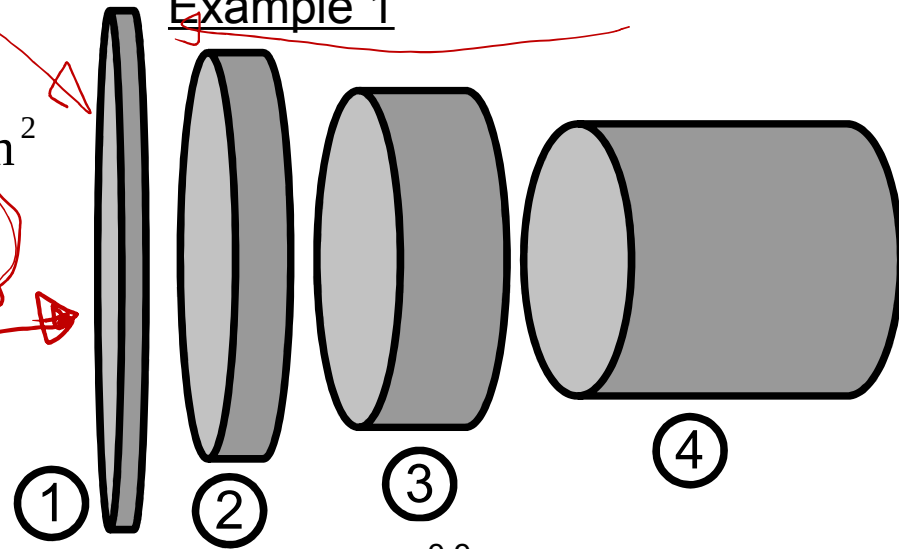
Solid cylinder

$$I_{FW} = \frac{1}{2} m r^2 = \frac{1}{2} \rho \pi h r^4 = 40 \text{ kgm}^2$$

$$\rho_{steel} = 7800 \text{ kg/m}^3$$

250 kg

1000 kg

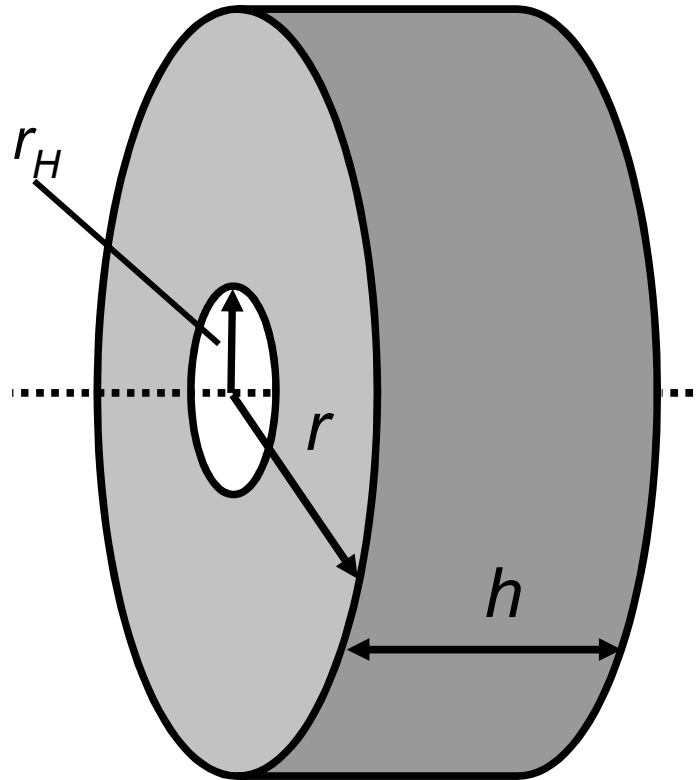


# Non-uniformity of machine motion

## Example 2

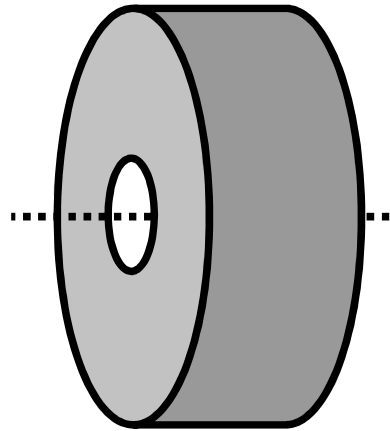
### Cylinder with a hole

$$I_{FW} = \frac{1}{2} \rho \pi h r^4 - \frac{1}{2} \rho \pi h r_H^4$$

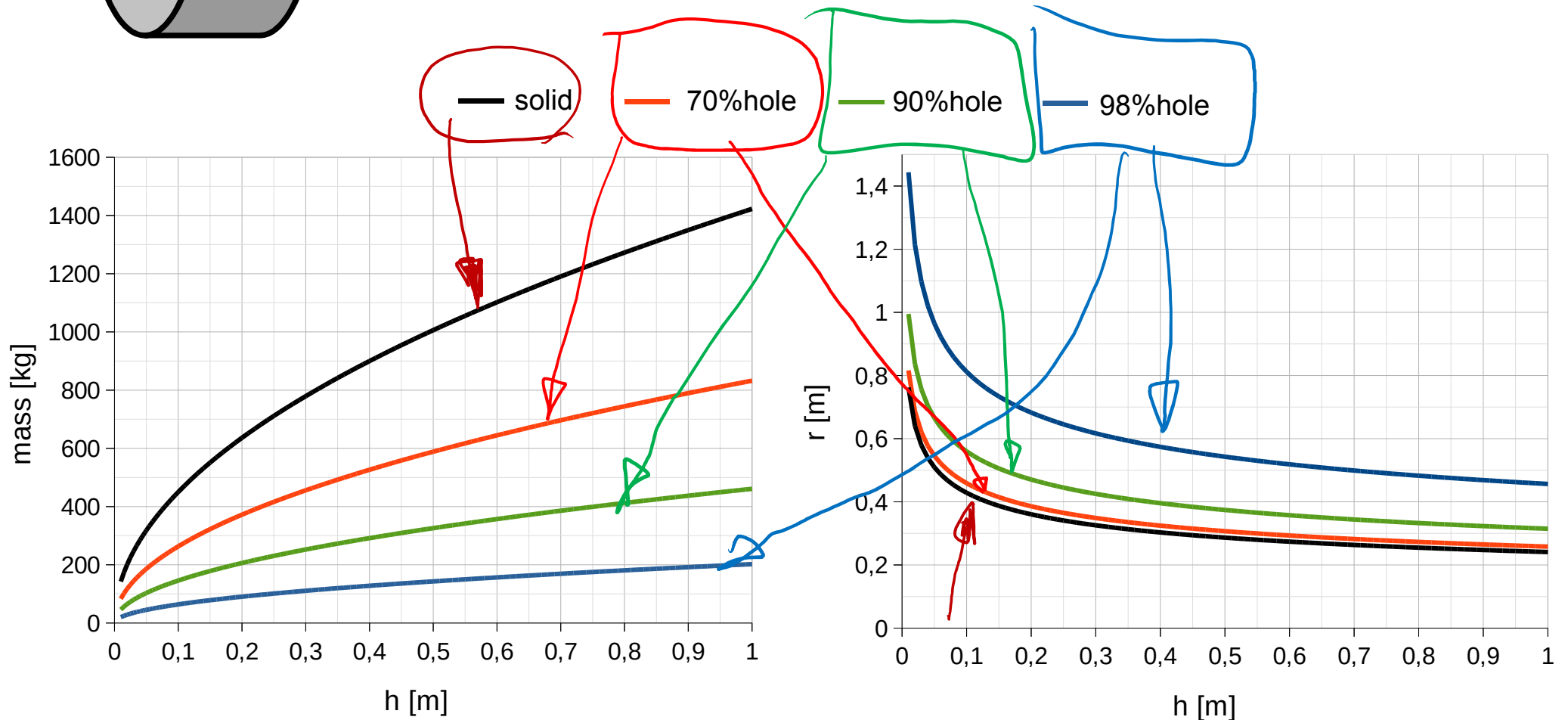


# Non-uniformity of machine motion

## Example 2 – cylinder with a hole



$$I_{FW} = \frac{1}{2} \rho \pi h r^4 - \frac{1}{2} \rho \pi h r_H^4 = 40 \text{ kgm}^2$$



# Non-uniformity of machine motion

Example 2 – cylinder with a hole

$$I_{FW} = \frac{1}{2} \rho \pi h r^4 - \frac{1}{2} \rho \pi h r_H^4 = 40 \text{ kgm}^2$$

	Solid cylinder	Cylinder 90% hole	Solid cylinder	Cylinder 98% hole
h=	10 cm	10 cm	5 cm	5 cm
r=	43 cm	56 cm	50 cm	96 cm
r <sub>H</sub> =	--	50.4 cm	--	94 cm
m=	442.8 kg	143.5 kg	313 kg	44.5 kg

+30%

+92%

-68%

-86%

# Non-uniformity of machine motion

To minimize flywheel's mass moment of inertia:

- you should mount a flywheel on a shaft that rotates with the highest angular velocity
- You can add extra transmission to increase angular velocity of a flywheel

# Automatic control

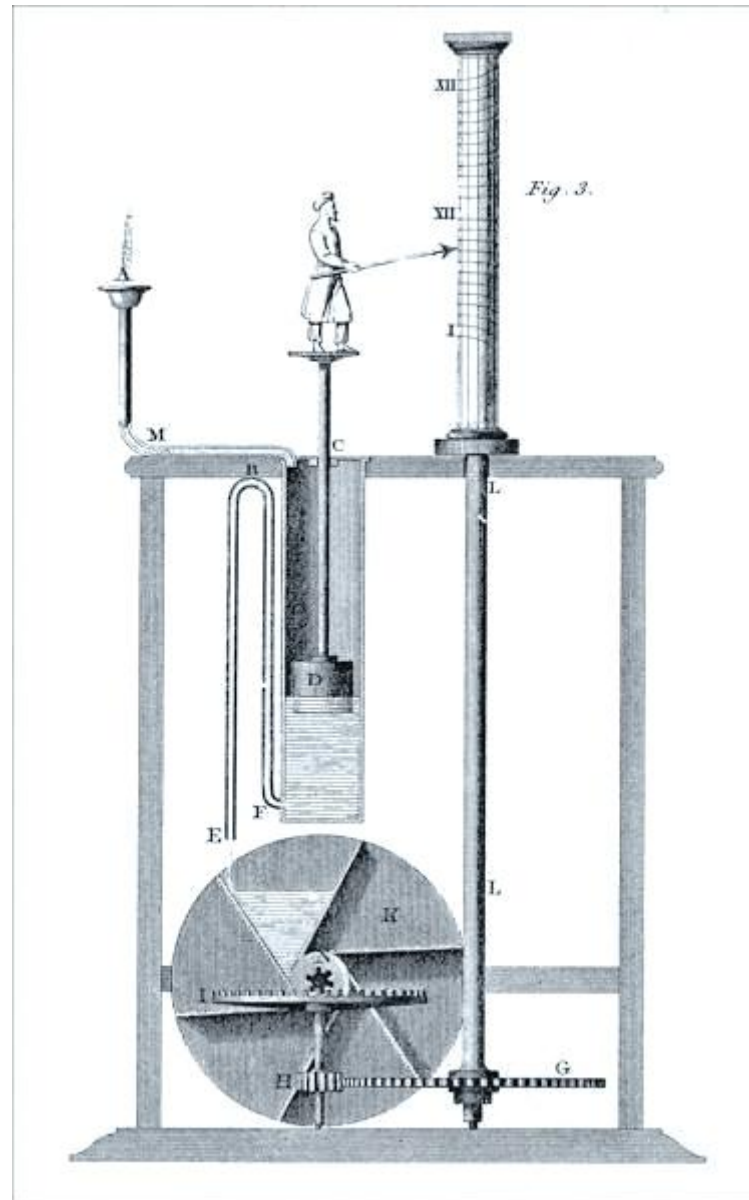
# Automatic control

“Automatic control in engineering and technology is a wide generic term covering the application of mechanisms to the operation and regulation of processes without continuous direct human intervention.” - *wikipedia*

Control theory – branch of mathematics and cybernetics that deals with analysis and mathematical modeling of objects and processes treated as dynamical systems with **feedback**.

# Automatic control history

## Ancient Greece, Arabs



**water clocks,  
automatic wine metering,  
door opening in temples**

Ctesibius's clepsydra (3rd century BC).

*Source-wikipedia: Abraham Rees (1819) "Clepsydra" in Cyclopædia: or, a New Universal Dictionary of Arts and Sciences The image is the JPEG reproduction published 2007-02-01 by the Horological Foundation.*

# Automatic control history

## XVII-XVIII

Temperature regulators for fireplaces and boilers  
pressure regulators for pressure cookers

## XVIII-XIX

float regulators for water distribution and steam engines  
velocity and force regulators for grain mills  
Watt's regulator for steam engines (centrifugal governor)

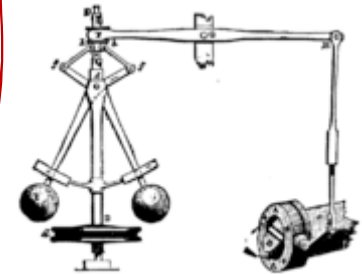


FIG. 4.—Governor and Throttle-Valve.

## XIX-XX

Laplace transform and Z-transform

Lyapunov stability theory

Routh stability criterion

Hurwitz stability criterion

Nyquist stability criterion and frequency domain analysis

Bode & Nichols frequency domain analysis

Evans root locus analysis

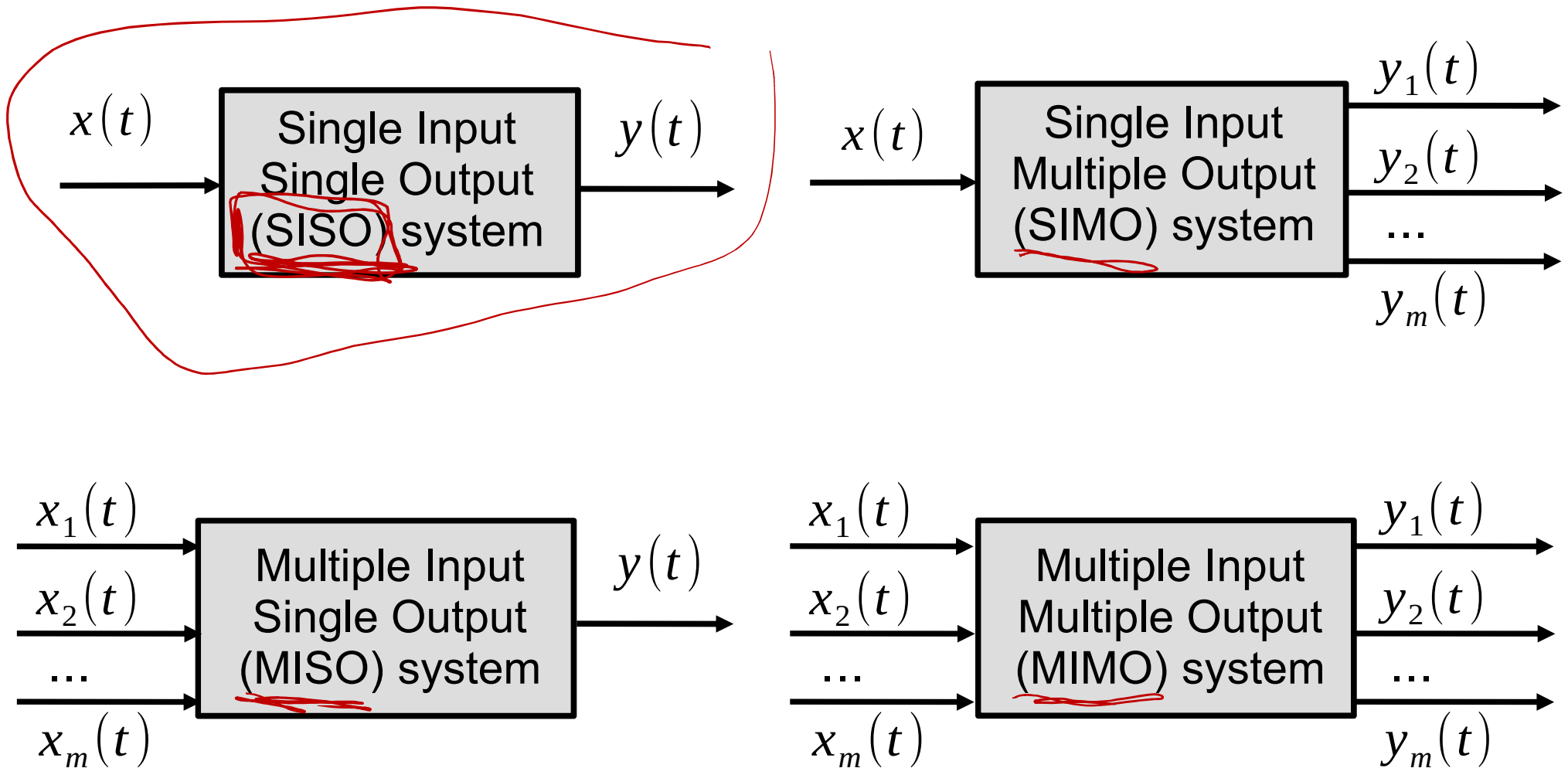
# Automatic control

<b>Classical control theory</b>	
<u>single input</u> , <u>single output</u> (SISO)	
usually <u>linear</u> systems	
<u>time independent</u> systems	
description by a <u>transfer functions</u>	
<u>time</u> and <u>frequency</u> domain analysis	
<u>system response</u> is the most important	

# Automatic control

<b>Classical control theory</b>	<b>modern control theory (1950-now)</b>
single input, single output (SISO)	multiple input, multiple output (MIMO)
usually linear systems	often <u>nonlinear systems</u>
time independent systems	<u>time dependent systems</u>
description by a transfer functions	description by a <u>state equations</u>
time and frequency domain analysis	<u>time domain analysis</u>
system response is the most important	system <u>state</u> is the most important

# Number of inputs and outputs



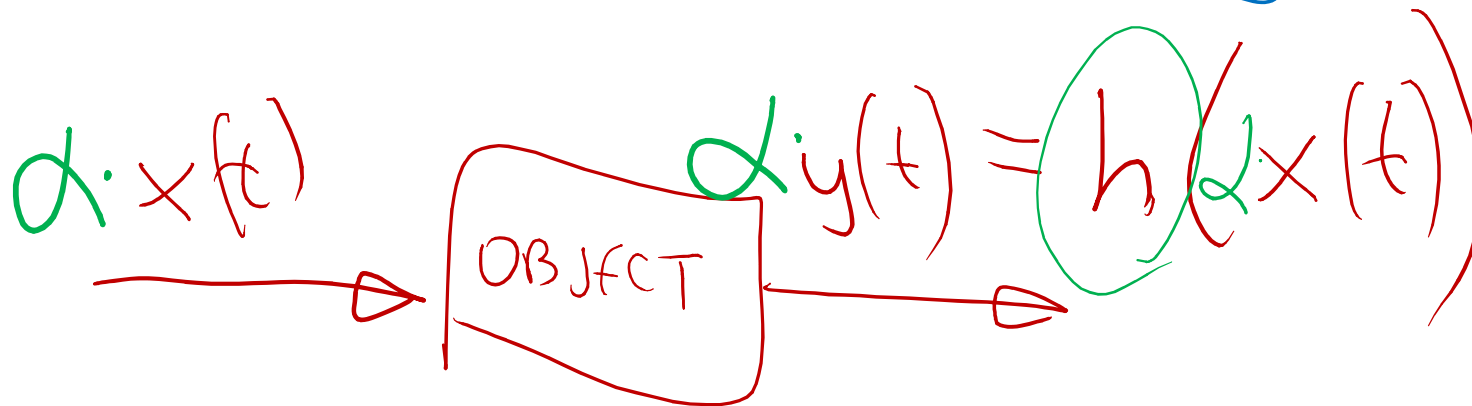
# Linear time-invariant (LTI) system

Linear system

$x(t)$  - input,  $y(t) = h(x(t))$  - output

$$h(\alpha x(t)) = \alpha h(x(t)) = \alpha y(t) \quad \text{scaling}$$

$$h(x_1(t) + x_2(t)) = h(x_1(t)) + h(x_2(t)) \quad \text{superposition}$$



# Linear time-invariant (LTI) system

## Time-invariant system

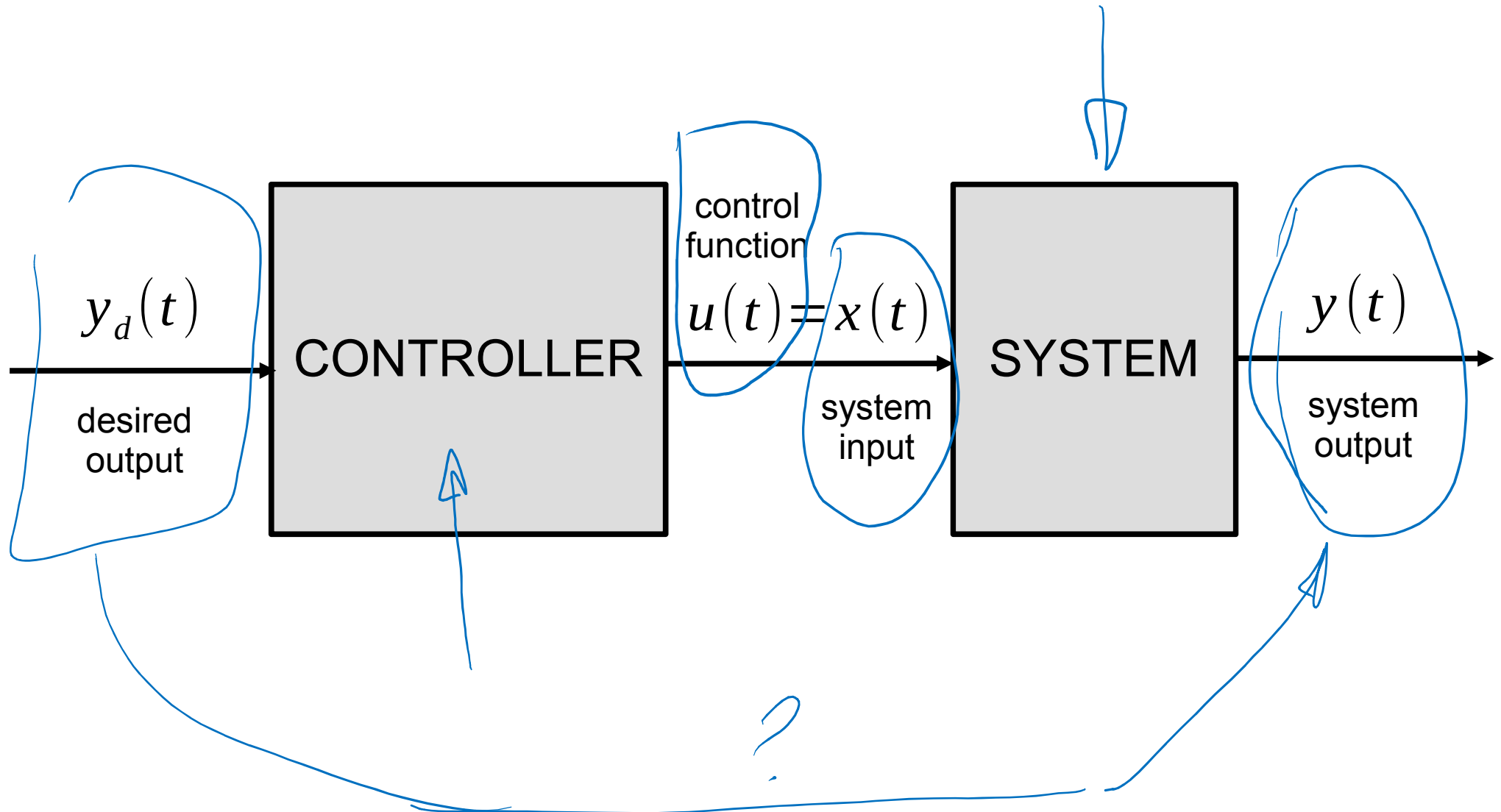
*output does not depend explicitly on time*

if  $y(t) = h(x(t))$  then  $y(t - \tau) = h(x(t - \tau))$

## Time-varying system

if  $y(t) = h(x(t))$  then  $y(t - \tau) \neq h(x(t - \tau))$

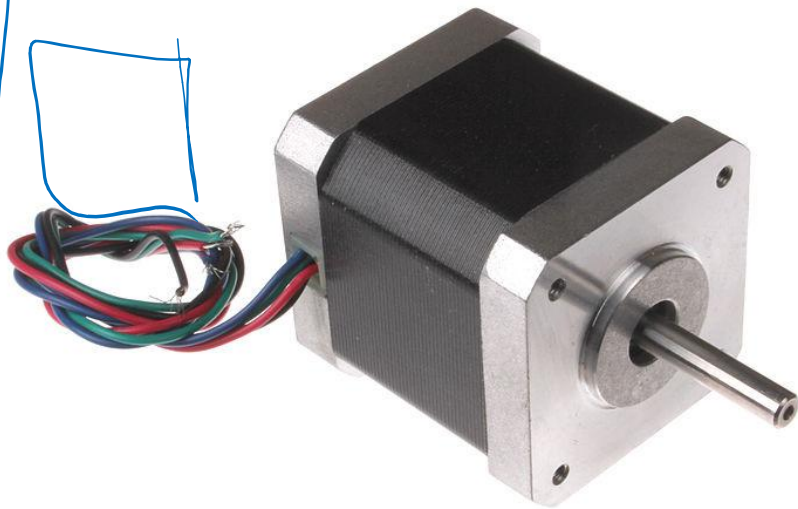
# Open loop control



# Open loop control

## Example usages

stepper motor



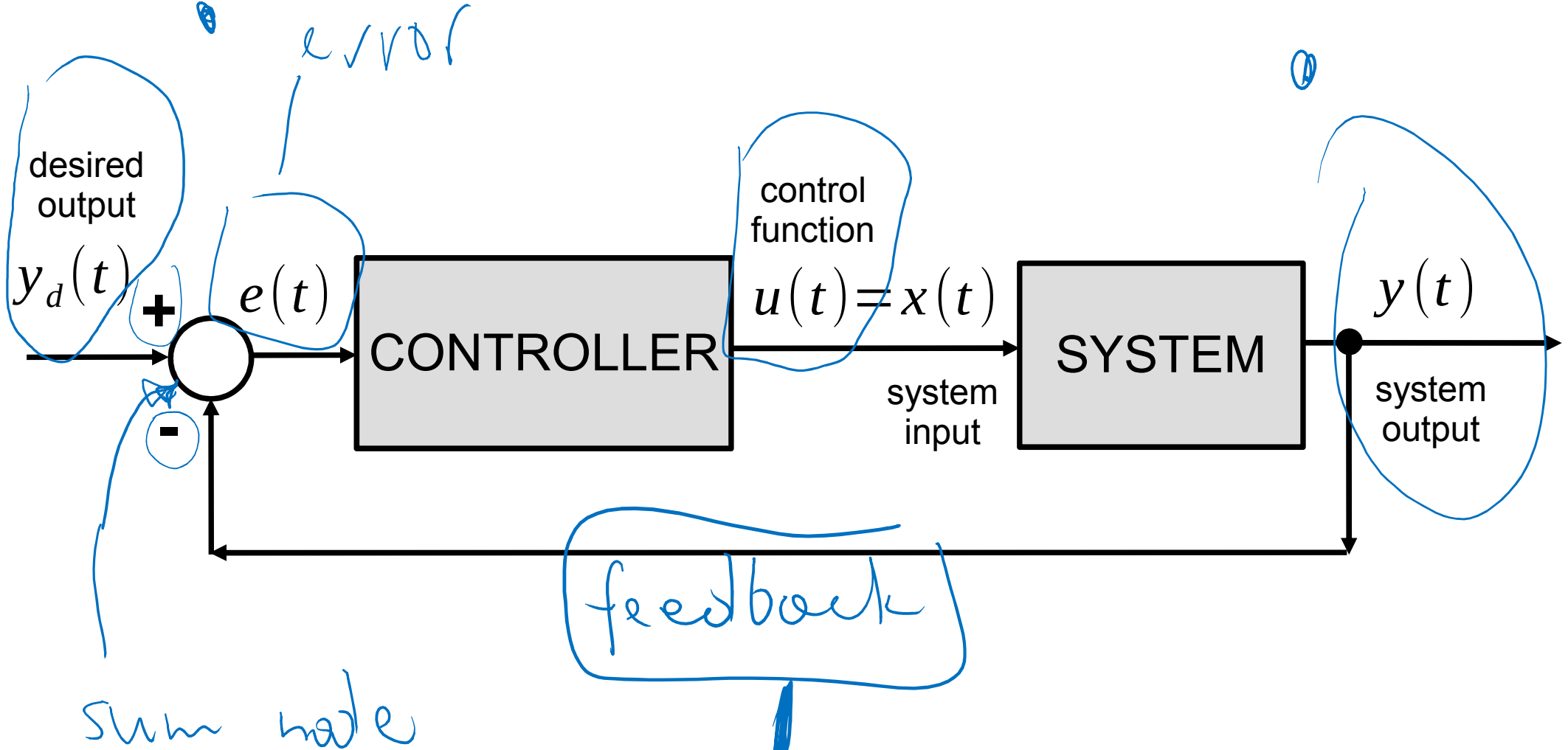
source: [wikimedia.org](http://wikimedia.org); author: oomlout

two wheeled platform  
(flat surface, no slip)

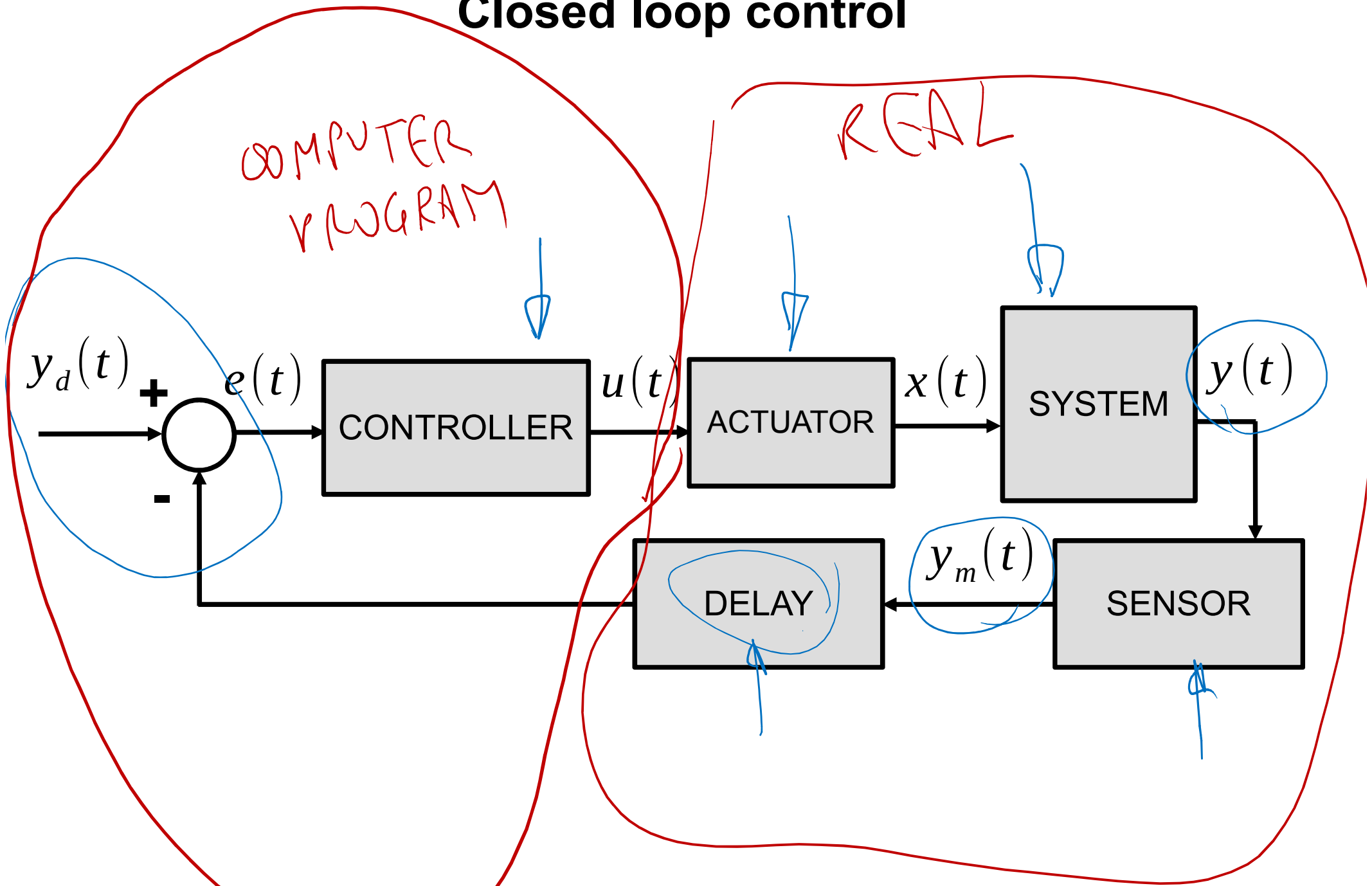


source: <http://www.robotliving.com>

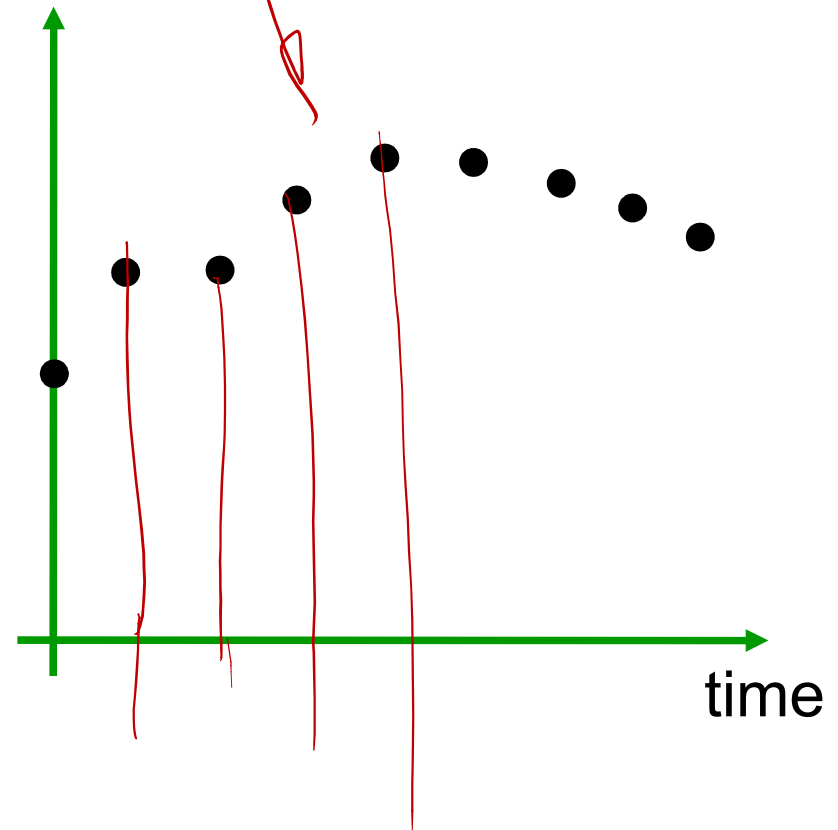
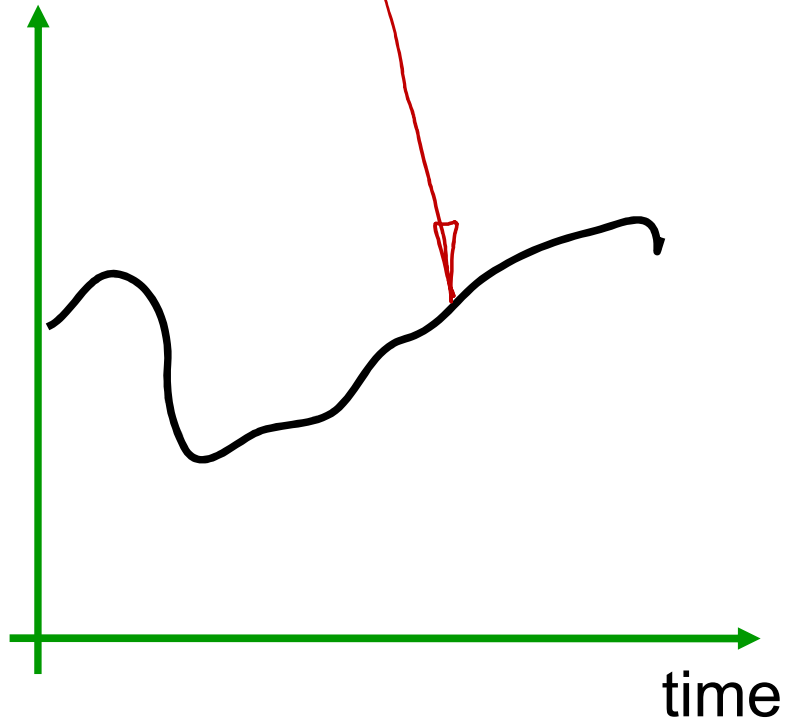
# Closed loop control



# Closed loop control



# Continuous/discrete signals



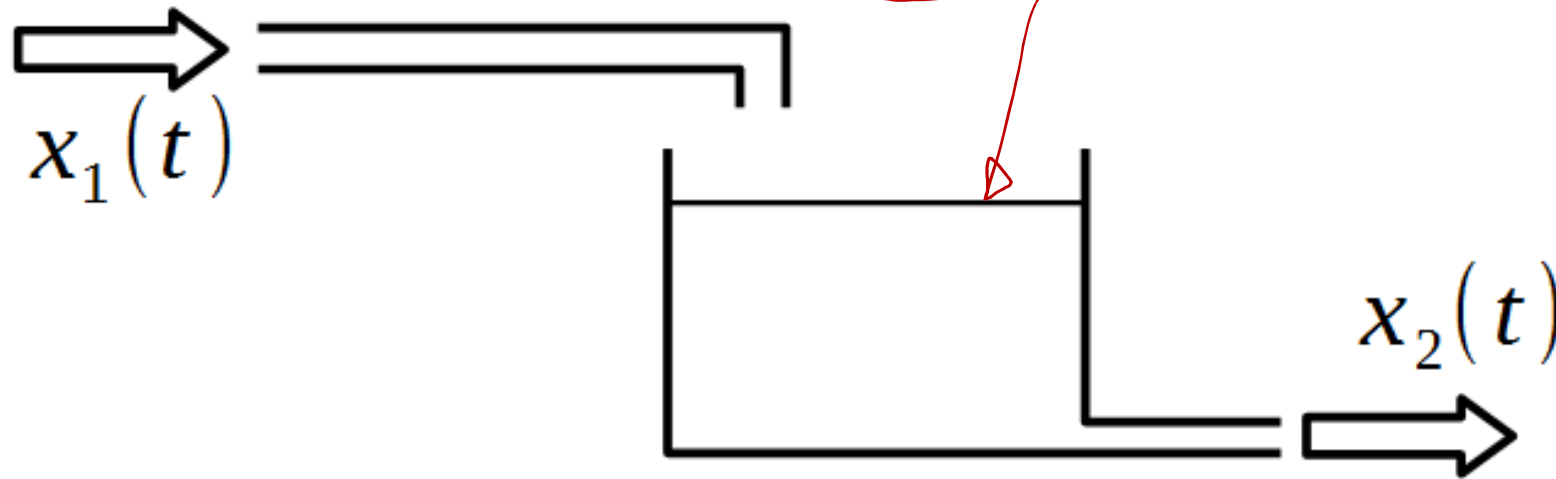
# Mathematical modeling of systems

- ↳ ordinary differential equations (ODEs)
- ↳ partial differential equations (PDEs)
- ↳ table representation
- ↳ recurrence equations
- ↳ stochastic representation
- ↳ neural networks
- ↳ logical
- arithmetic
- integral equations
- combination of above
- ...



# Mathematical modeling of systems

Example 1 – cylindrical tank



$x_1(t)[m^3/s]$  - inflow of a liquid

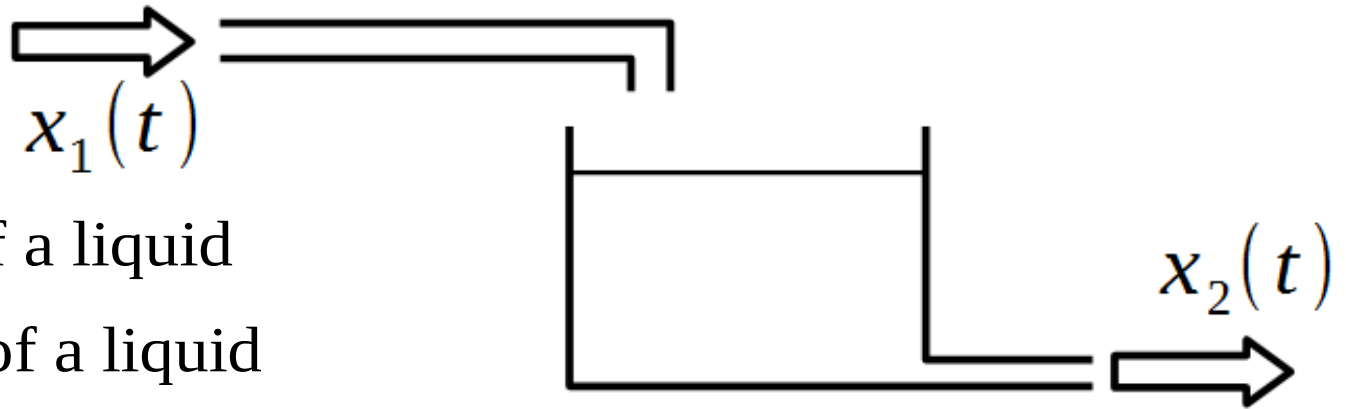
$x_2(t)[m^3/s]$  - outflow of a liquid

$v(t)[m^3]$  - volume of a liquid in a tank

Question: find out a relation between inflow, outflow and volume.

# Mathematical modeling of systems

## Example 1 – cylindrical tank



$x_1(t)$  [ $m^3/s$ ] - inflow of a liquid

$x_2(t)$  [ $m^3/s$ ] - outflow of a liquid

$v(t)$  [ $m^3$ ] - volume of a liquid in a tank

Question: find out a relation between inflow, outflow and volume.

$$v(t_1) \rightarrow v(t_1 + \Delta t) = v(t_1) + (x_1(t_1) - x_2(t_1)) \Delta t$$

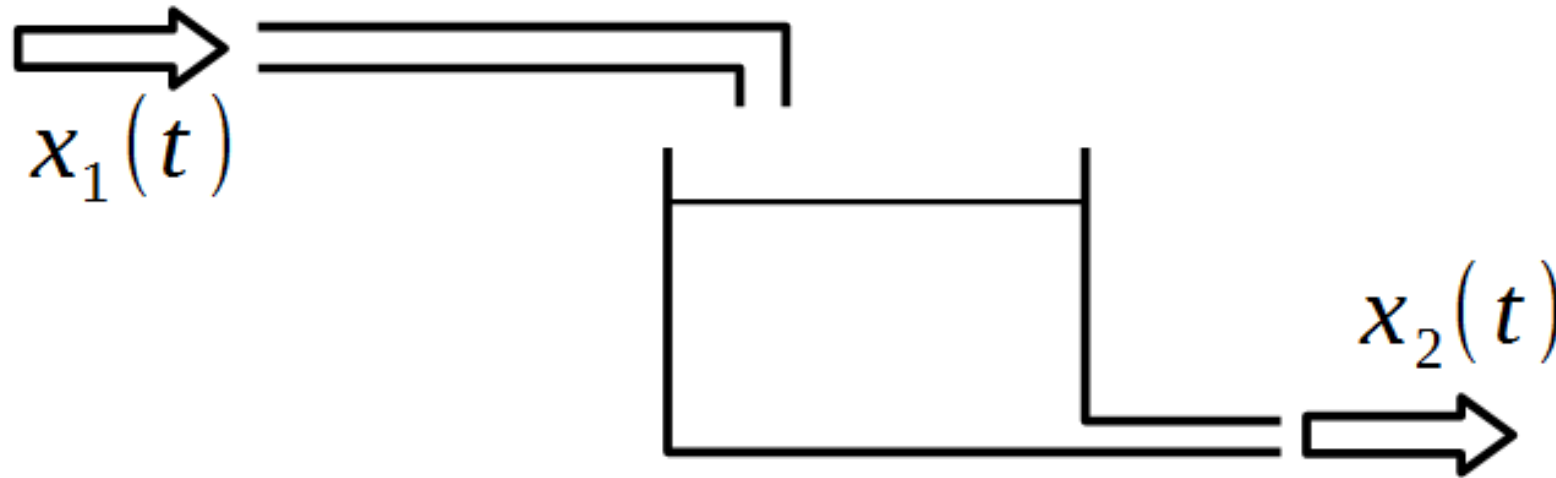
$$\frac{v(t_1 + \Delta t) - v(t_1)}{\Delta t} = x_1(t_1) - x_2(t_1)$$

$$\Delta t \rightarrow 0$$

$$\frac{dv(t)}{dt} = x_1(t) - x_2(t)$$

# Mathematical modeling of systems

## Example 1



$x_1(t)$  [ $m^3/s$ ] - inflow of a liquid

$x_2(t)$  [ $m^3/s$ ] - outflow of a liquid

$v(t)$  [ $m^3$ ] - volume of a liquid in a tank

Question: find out a relation between inflow, outflow and volume.

Answer:

$$t_2 = t_1 + \Delta$$

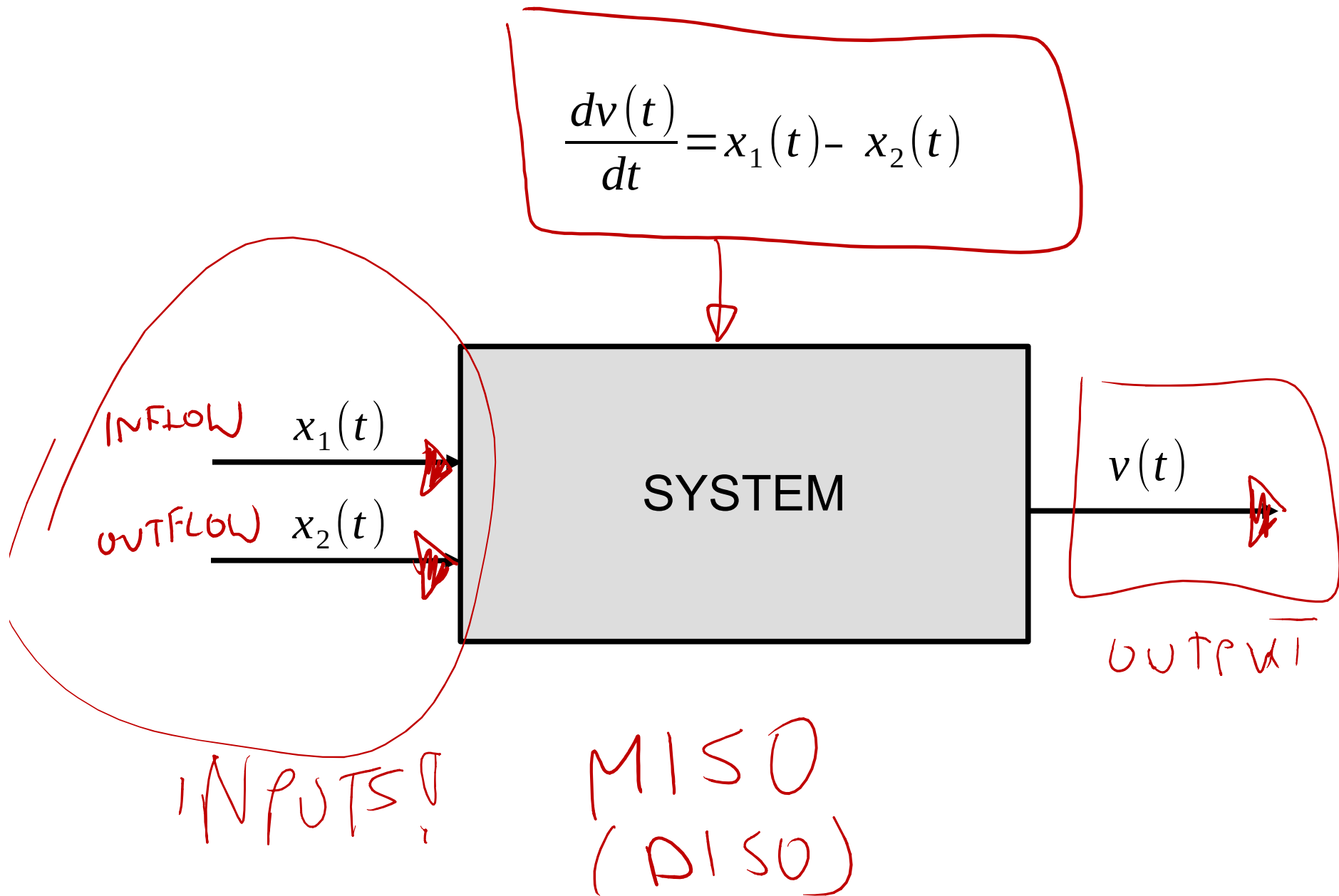
$$v(t_2) \approx v(t_1) + \Delta (x_1(t_2) - x_2(t_2))$$

$$\frac{v(t_2) - v(t_1)}{\Delta} \approx x_1(t_2) - x_2(t_2)$$

$$\frac{dv(t)}{dt} = x_1(t) - x_2(t)$$

# Mathematical modeling of systems

## Example 1



# Mathematical modeling of systems

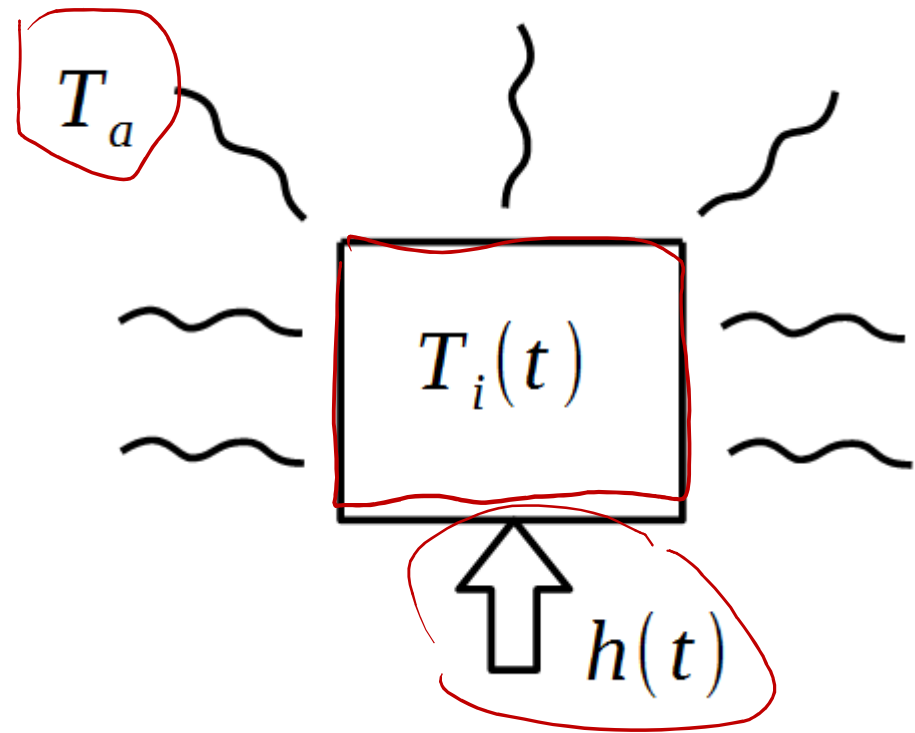
## Example 2

$h(t)[W]$  - heater power

$T_a(t)[K]$  - ambient temperature

$T_i(t)[K]$  - object temperature

Question: how to obtain a relation between heater power (input) and object temperature (output)?  
Assume energy loss only by convection.



# Mathematical modeling of systems

## Example 2

Answer:

$$\text{rate of change of heat} = \text{heat gain} - \text{heat loss}$$

# Mathematical modeling of systems

## Example 2

Answer:

rate of change of heat = heat gain – heat loss

$$\frac{dQ(t)}{dt} = \underline{Q_H} - \underline{Q_L}$$

# Mathematical modeling of systems

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$c_p [J/kg K]$  - specific heat coefficient,  $m [kg]$  - mass of the object

# Mathematical modeling of systems

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# Mathematical modeling of systems

## Example 2

Answer:

rate of change of heat = heat gain - heat loss

$$\frac{dQ(t)}{dt} = Q_H - Q_L$$

$$c_p m \frac{dT_i(t)}{dt} + \alpha T_i(t) = h(t) + \alpha T_a(t)$$

$Q [J] = c_p m T_i$  - heat energy inside the object

$c_p [J/kg K]$  - specific heat coefficient,  $m [kg]$  - mass of the object

$Q_H [W] = h(t)$  - increase of heat energy caused by the heater

$Q_L [W] = \alpha (T_i - T_a)$  - heat energy loss caused by convection

$\alpha [W/K]$  - convection coefficient (assume constant)

$$c_p m \frac{dT_i(t)}{dt} = h(t) - \alpha (T_i(t) - T_a(t))$$

# Mathematical modeling of systems

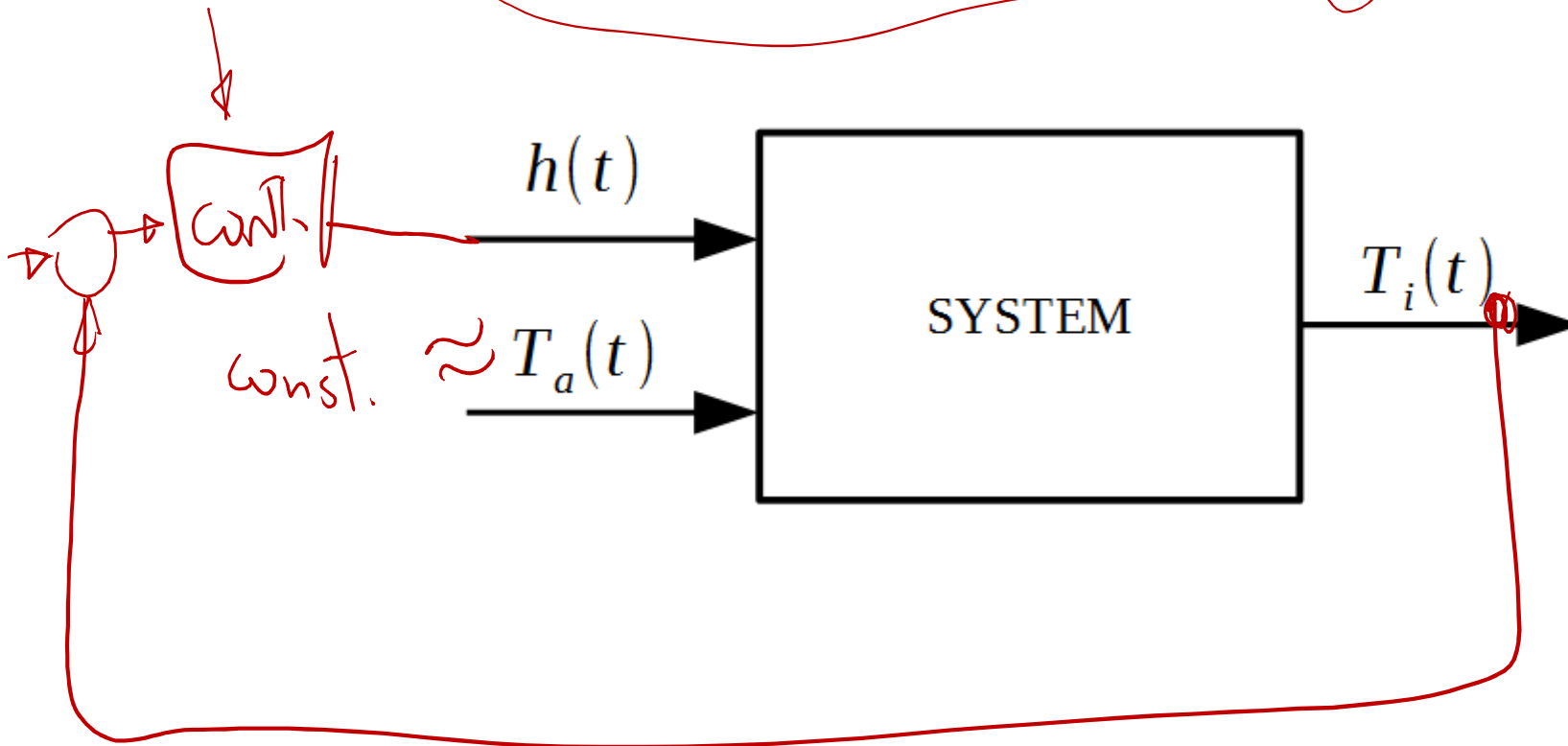
## Example 2

$$c_p m \frac{dT_i(t)}{dt} = h(t) - \alpha (T_i(t) - T_a(t))$$

# Mathematical modeling of systems

## Example 2

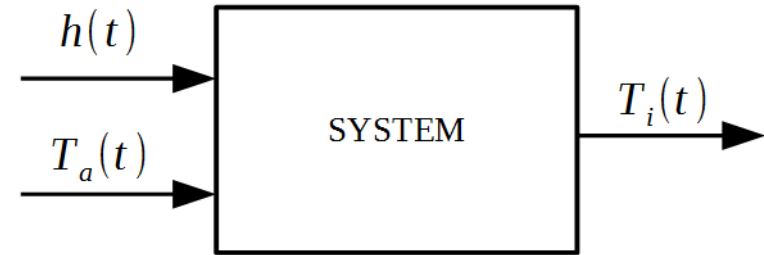
$$c_p m \frac{dT_i(t)}{dt} = h(t) - \alpha (T_i(t) - T_a(t))$$



# Mathematical modeling of systems

## Example 2

$$c_p m \frac{dT_i(t)}{dt} = h(t) - \alpha(T_i(t) - T_a(t))$$



Question: Can we convert this MISO model into SISO model?